Concorde Glass Ltd.,

Linx House,

104 Waterloo Rd,

Mablethorpe,

LN12 1LE,

UK.

Glassloc Fixing & Wind Load Data

1507-1

Analysis By	Checked By
C.K. & R.F.	T.S.

1	12/04/2021	T.S	Amended
0	11/03/2021	T.S.	Issued
Revision	**Date**	**Issued By**	**Comment**

Contents

Introduction/Actions/Result Summary:

Introduction:

TSA was instructed by Concorde Glass Ltd to provide a matrix of wind load for a top mounted shoe type.

Actions:

Infill load = 1.0kN/m² (Table NA.5 IS1991-1-1:2002)
Point load = 0.5kN (Table NA.5 IS1991-1-1:2002)
Wind load = 1.0kN/m²

Assumption:

Concrete Grade = C30/37

Timber Grade = C16 (minimum)

Result Summary:

Connection to Concrete: Use 1Nr Fischer Threaded rod FIS A M 10×110 with FIS V 360 S Fischer Chemical Resin @200mm C/C with a minimum of 45mm Concrete edge distance.

Connection to Steel: Use 1Nr M12 Grade 8.8 bolts @600mm C/C.

Connection to Wood: Use 1Nr TB M12×60mm Index Wood Screws @200mm C/C.

Glass Analysis					
Case Study	Glass (mm)	Interlayer -	Wind Load - Qw (kN/m²)	Height glass (m)	Glass Deflection (mm)
1	12		1.0	1.100	11.63
2	15		1.0	1.100	5.957
3	17.52	EVA	1.0	1.100	5.222
4	21.52	EVA	1.0	1.100	2.903

Notes:

1- All systems are suitable for Low and Medium wind load.
2- All Systems have Concrete, Steel and Timber fixings included in the Report.
3- The Maximum Glass Width is 1000mm, and the Maximum Glass Height is 1100mm.

Glass Strength

Wind Loading:

10min duration, Multiple Gust Storm => k_{mod} = 0.74

$f_{gd} = (k_{mod})(k_{sp})(f_{gk})/\ \gamma_{ma} + k_v(f_{bk}-f_{gk})/\gamma_{mv}$

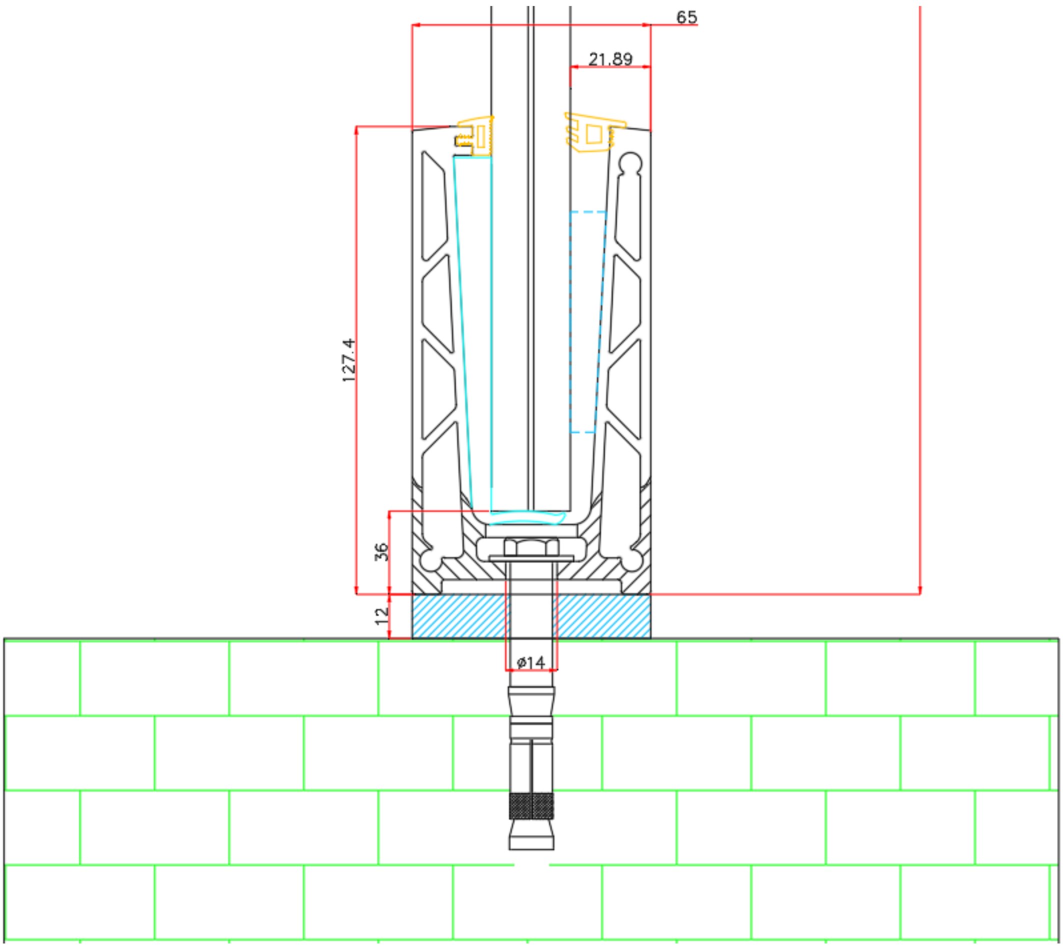
$f_{gd} = (0.74)(1.0)(45)/1.6 + 1.0(120-45)/1.2$

<u>f_{gd} = 83.3N/mm^2</u>

Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 5
Date: 11/03/2021	By: C.K. & R.F.

System Sketch:

Concorde Glass Ltd Top Mounted Shoe:



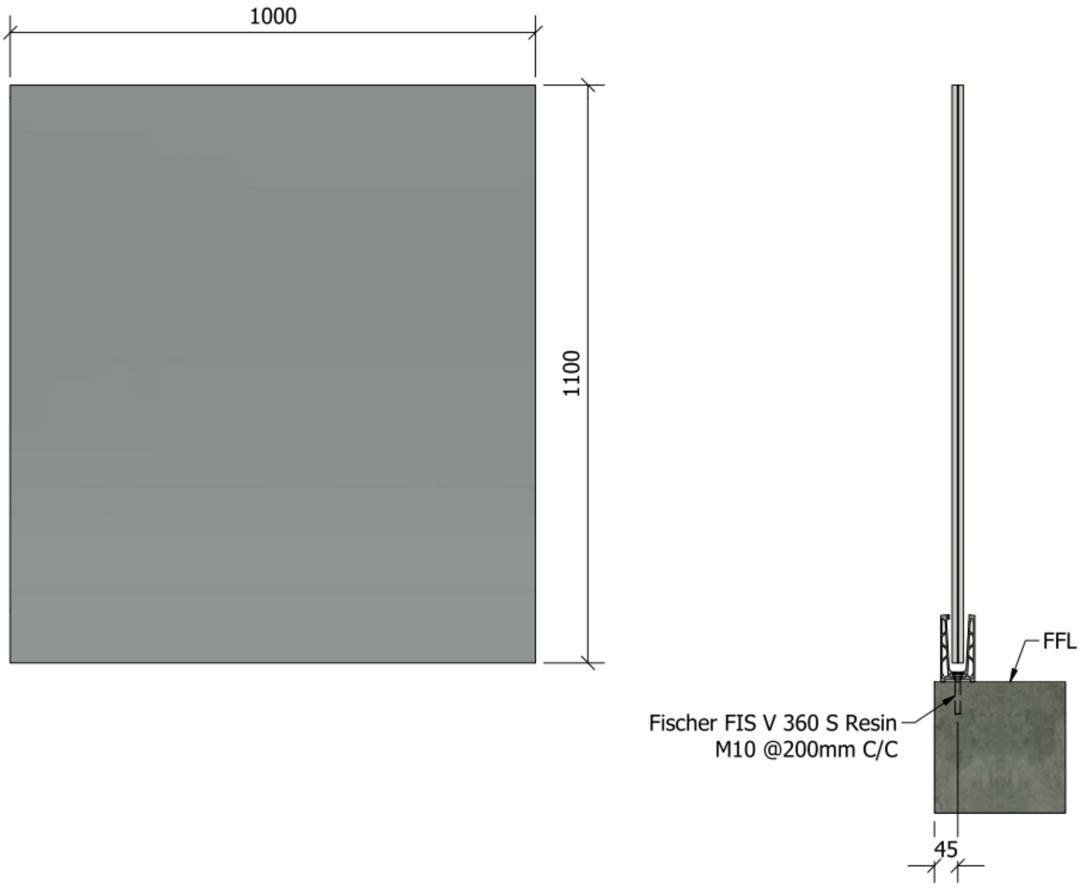
Project: Concorde Glass Ltd.	**Contract:** 1507-1
Subject: Glassloc Fixing & Wind Load Data	**Sheet No.** 6
Date: 11/03/2021	**By:** C.K. & R.F.

Case Study 01: 12mm Toughened Glass – 1.0x1.100m – 1.0kN/m^2

Case Study 02: 15mm Toughened Glass – 1.0x1.100m – 1.0kN/m^2

Case Study 03: 17.52mm Laminated Toughened Glass – 1.0x1.100m – 1.0kN/m^2

Case Study 04: 21.52mm Laminated Toughened Glass – 1.0x1.100m – 1.0kN/m^2



Glass & Shoe Analysis:

Glass Analysis – 12mm:

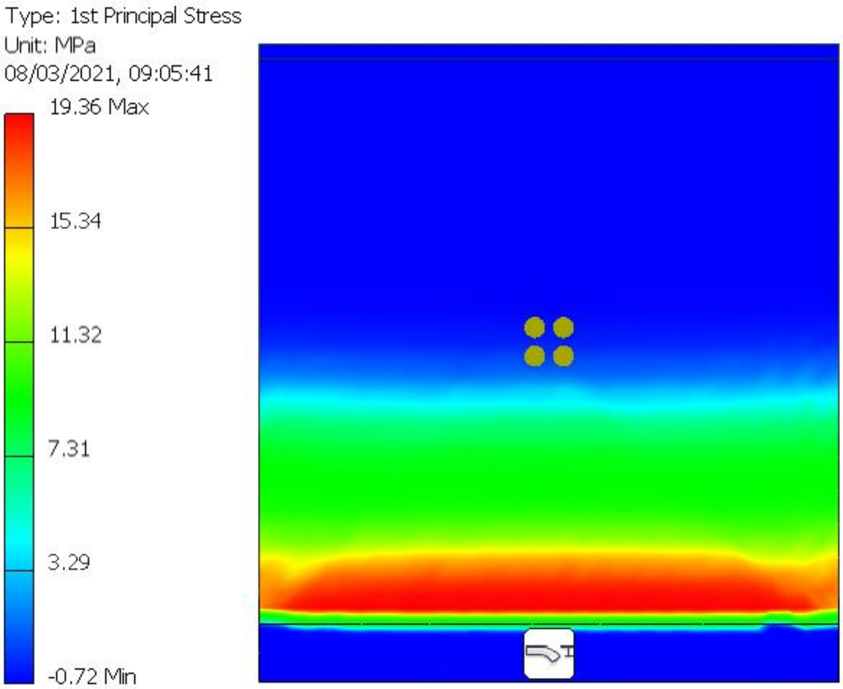
Glass Analysis - Bending Stress of Glass Panel due to 1.0kN/m2 Infill Loading:

- Analysis Software was used to determine maximum bending stress of the glass due to 1.0N/m2 Infill Loading
- 12mm Toughened Glass
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 19.36N/mm^2 X 1.5 = 29.04N/mm^2 < 84.2N/mm^2

OK in Bending



	Project: Concorde Glass Ltd.	Contract: 1507-1
TSA TED SINGLETON & ASSOCIATES CONSULTING ENGINEERS	Subject: Glassloc Fixing & Wind Load Data	Sheet No. 8
	Date: 11/03/2021	By: C.K. & R.F.

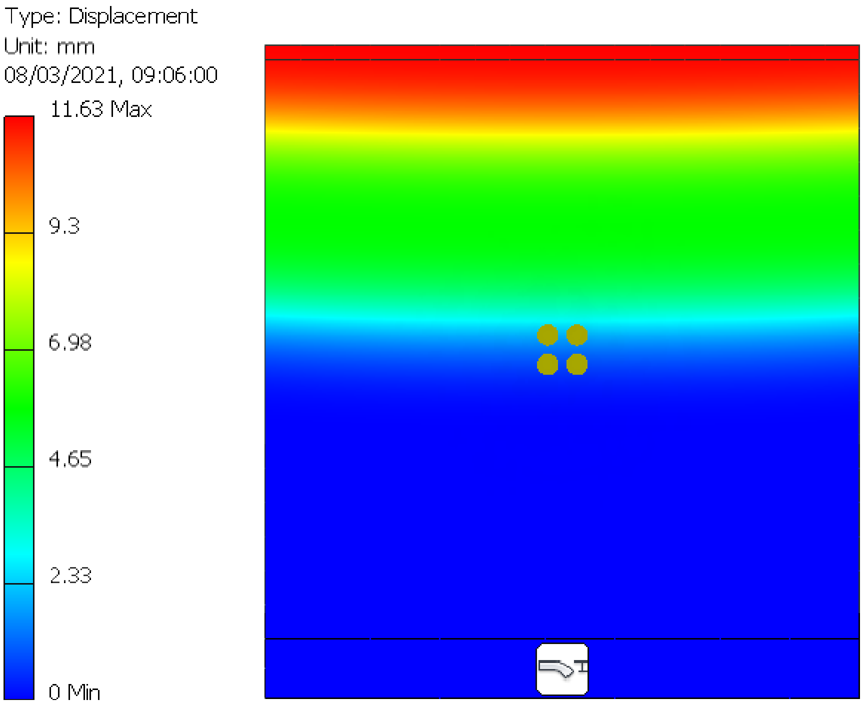
Glass Analysis - Deflection of Glass Panel due to 1.0kN/m2 Infill Loading:

- Analysis Software was used to determine maximum deflection of the glass due to 1.0N/m2 Infill Loading
- 12mm Toughened Glass
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 11.63mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



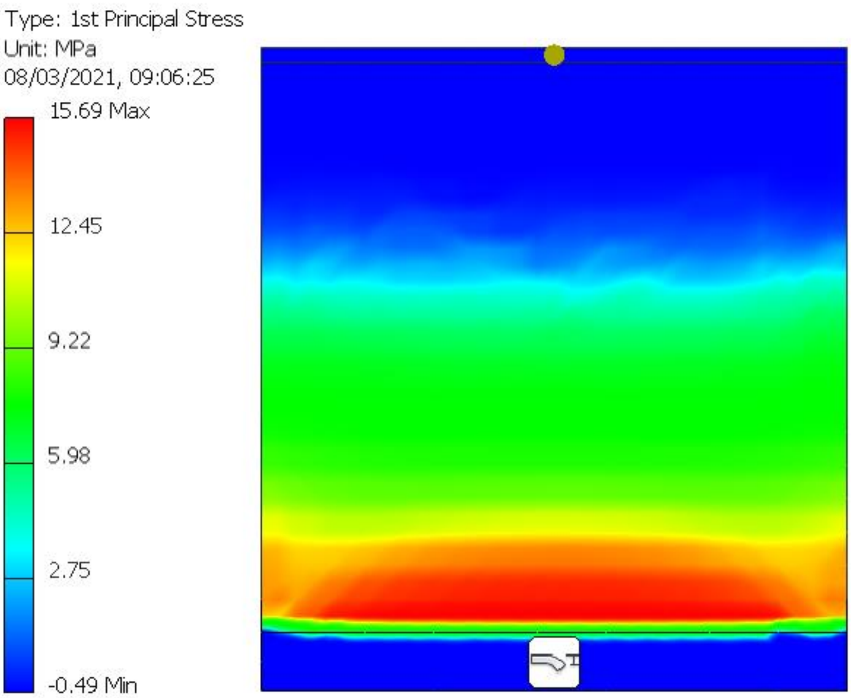
Glass Analysis - Bending Stress of Glass Panel due to 0.36kN/m Balustrade Loading:

- Analysis Software was used to determine maximum bending stress of the glass due to 0.36kN/m Balustrade Loading
- 12mm Toughened Glass
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 15.69N/mm^2 X 1.5 = 23.535N/mm^2 < 84.2N/mm^2

OK in Bending



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 10
Date: 11/03/2021	By: C.K. & R.F.

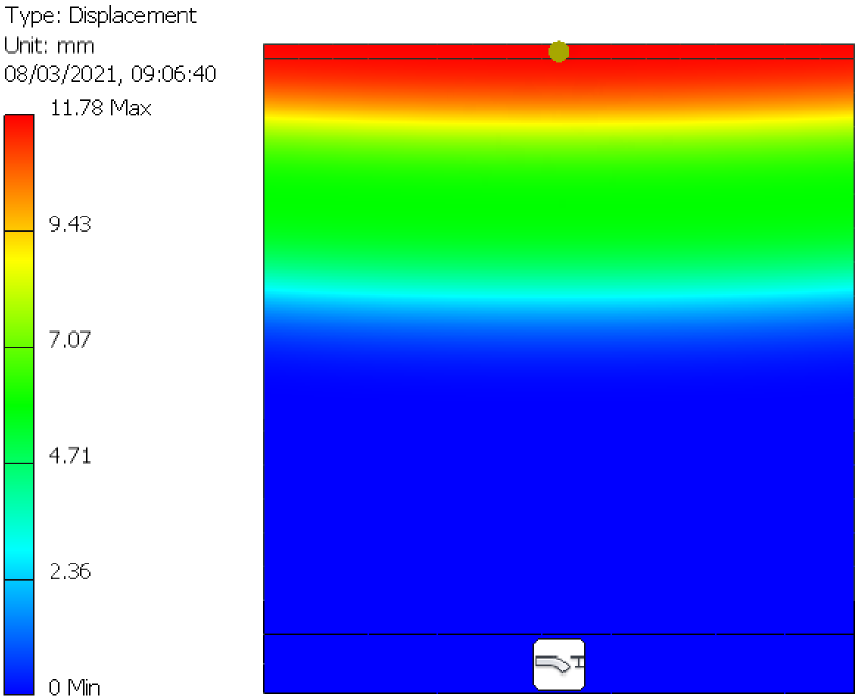
Glass Analysis - Deflection of Glass Panel due to 0.36kN/m Balustrade Loading:

- Analysis Software was used to determine maximum deflection of the glass due to 0.36kN/m Balustrade Loading
- 12mm Toughened Glass
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 11.78mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



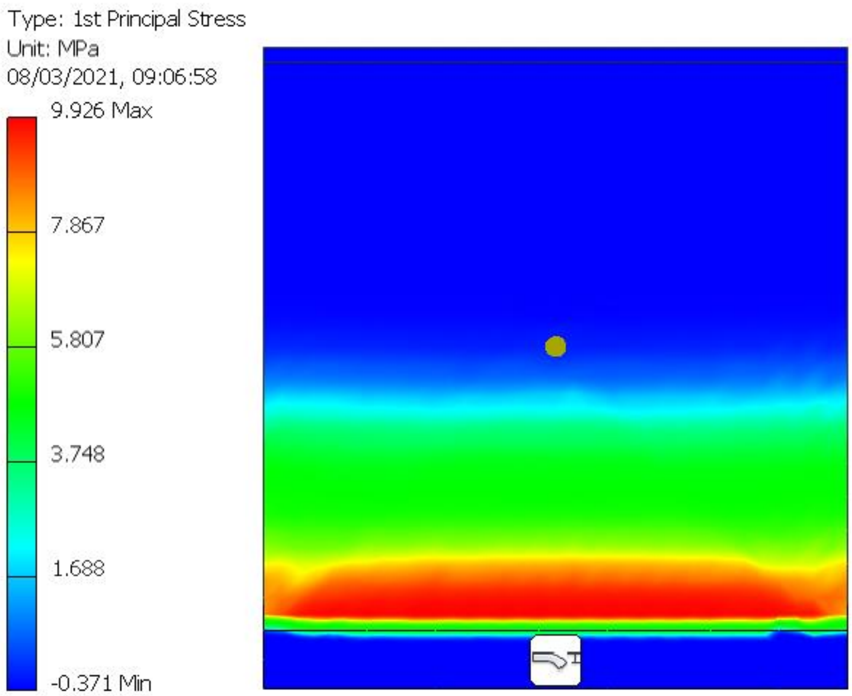
Glass Analysis - Bending Stress of Glass Panel due to 0.5kN Point Load:

- Analysis Software was used to determine maximum bending stress of the glass due to 0.5kN Point Load
- 12mm Toughened Glass
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 9.926N/mm^2 X 1.5 = 14.889N/mm^2 < 84.2N/mm^2

OK in Bending



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 12
Date: 11/03/2021	By: C.K. & R.F.

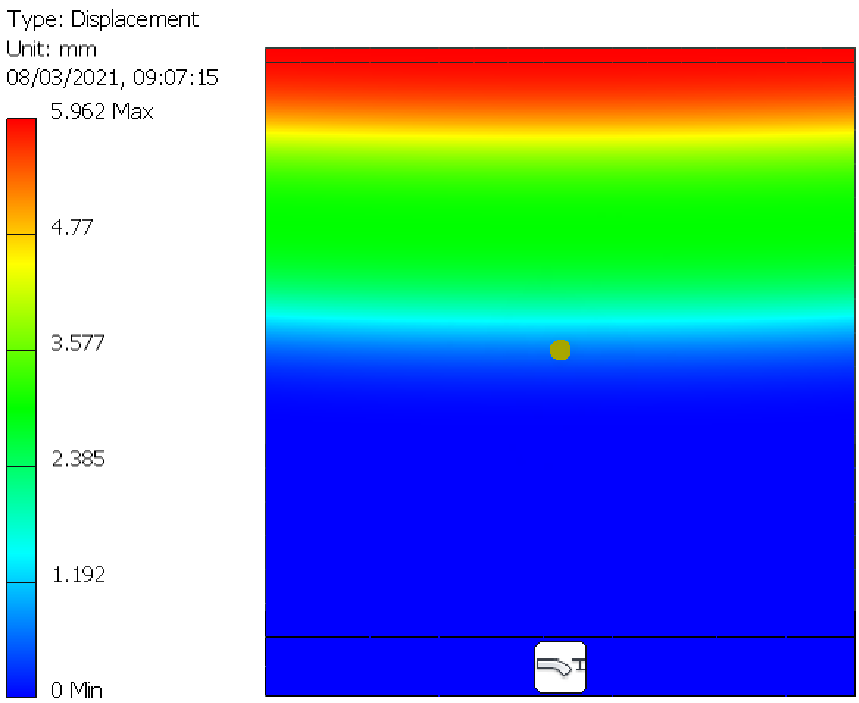
Glass Analysis - Deflection of Glass Panel due to 0.5kN Point Load:

- Analysis Software was used to determine maximum deflection of the glass due to 0.5kN Point Load
- 12mm Toughened Glass
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 5.962mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



TSA TED SINGLETON & ASSOCIATES CONSULTING ENGINEERS	**Project:** Concorde Glass Ltd.	**Contract:** 1507-1
	Subject: Glassloc Fixing & Wind Load Data	**Sheet No.** 13
	Date: 11/03/2021	**By:** C.K. & R.F.

Glass Analysis – 15mm:

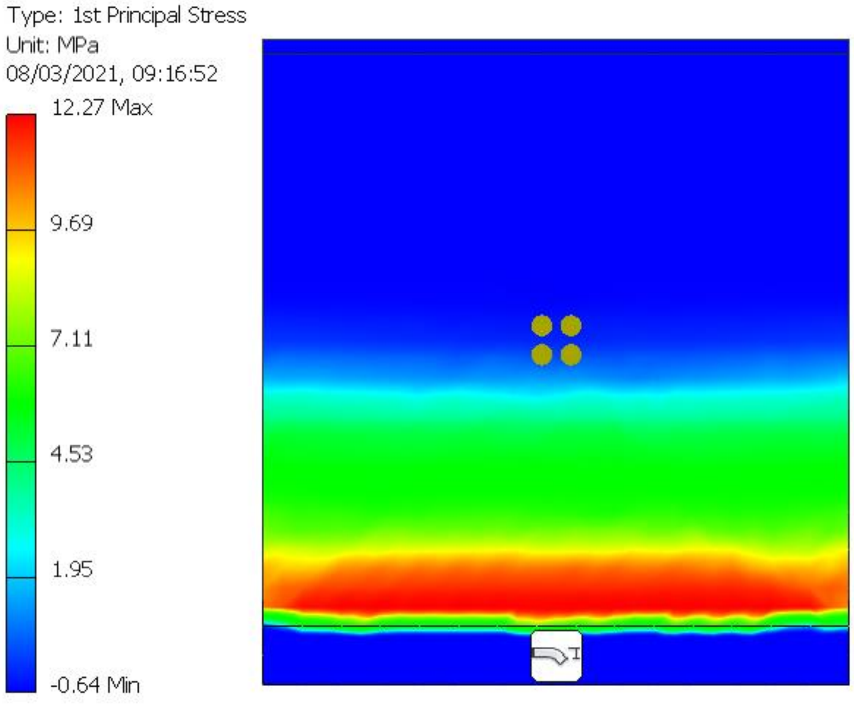
Glass Analysis - Bending Stress of Glass Panel due to 1.0kN/m2 Infill Loading:

- Analysis Software was used to determine maximum bending stress of the glass due to 1.0N/m2 Infill Loading
- 15mm Toughened Glass
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 12.27N/mm^2 X 1.5 = 18.405N/mm^2 < 84.2N/mm^2

OK in Bending



TSA
TED SINGLETON & ASSOCIATES
CONSULTING ENGINEERS

Project: Concorde Glass Ltd.	**Contract:** 1507-1
Subject: Glassloc Fixing & Wind Load Data	**Sheet No.** 14
Date: 11/03/2021	**By:** C.K. & R.F.

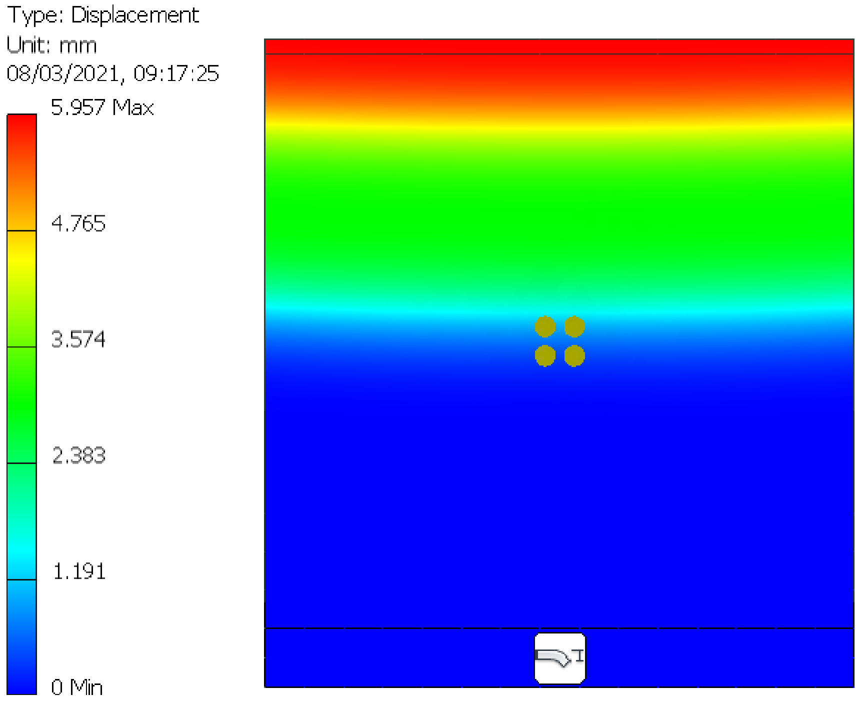
Glass Analysis - Deflection of Glass Panel due to 1.0kN/m2 Infill Loading:

- Analysis Software was used to determine maximum deflection of the glass due to 1.0N/m2 Infill Loading
- 15mm Toughened Glass
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 5.957mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 15
Date: 11/03/2021	By: C.K. & R.F.

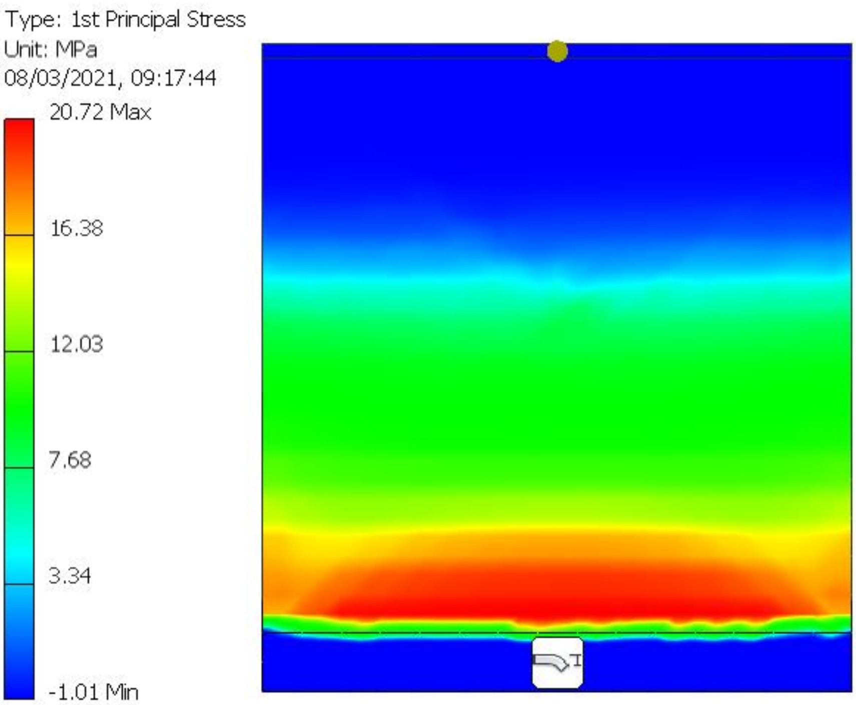
Glass Analysis - Bending Stress of Glass Panel due to 0.74kN/m Balustrade Loading:

- Analysis Software was used to determine maximum bending stress of the glass due to 0.74kN/m Balustrade Loading
- 15mm Toughened Glass
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 20.72N/mm^2 X 1.5 = 31.08N/mm^2 < 84.2N/mm^2

OK in Bending



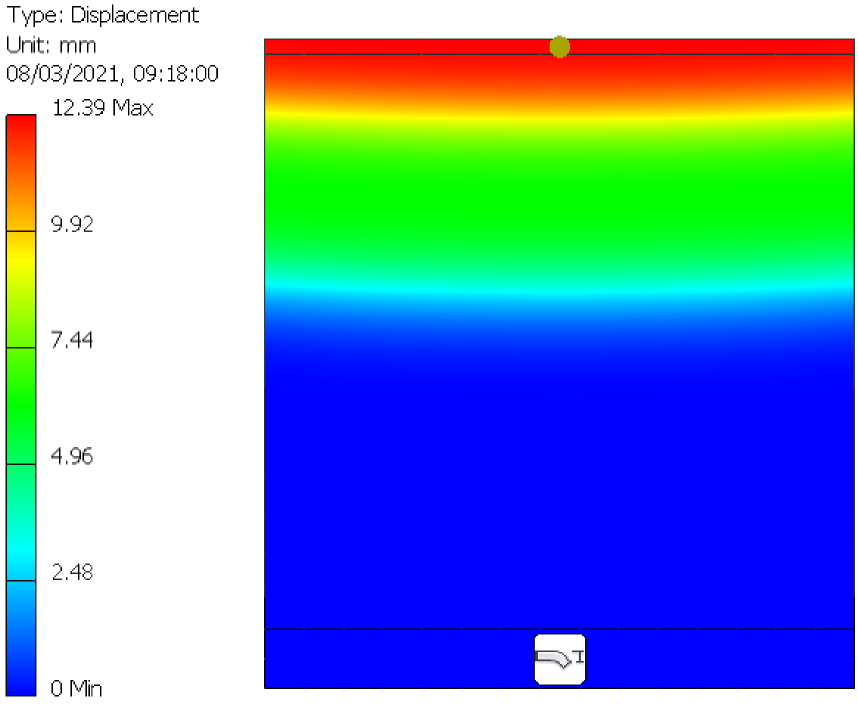
Glass Analysis - Deflection of Glass Panel due to 0.74kN/m Balustrade Loading:

- Analysis Software was used to determine maximum deflection of the glass due to 0.74kN/m Balustrade Loading
- 15mm Toughened Glass
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 12.39mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 17
Date: 11/03/2021	By: C.K. & R.F.

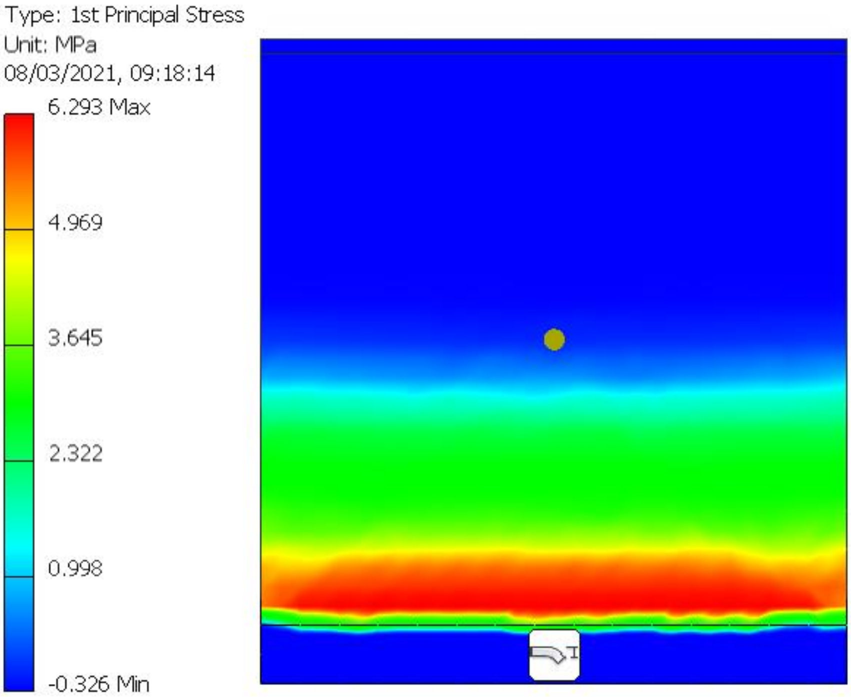
Glass Analysis - Bending Stress of Glass Panel due to 0.5kN Point Load:

- Analysis Software was used to determine maximum bending stress of the glass due to 0.5kN Point Load
- 15mm Toughened Glass
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 6.293N/mm^2 X 1.5 = 9.4395N/mm^2 < 84.2N/mm^2

OK in Bending



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 18
Date: 11/03/2021	By: C.K. & R.F.

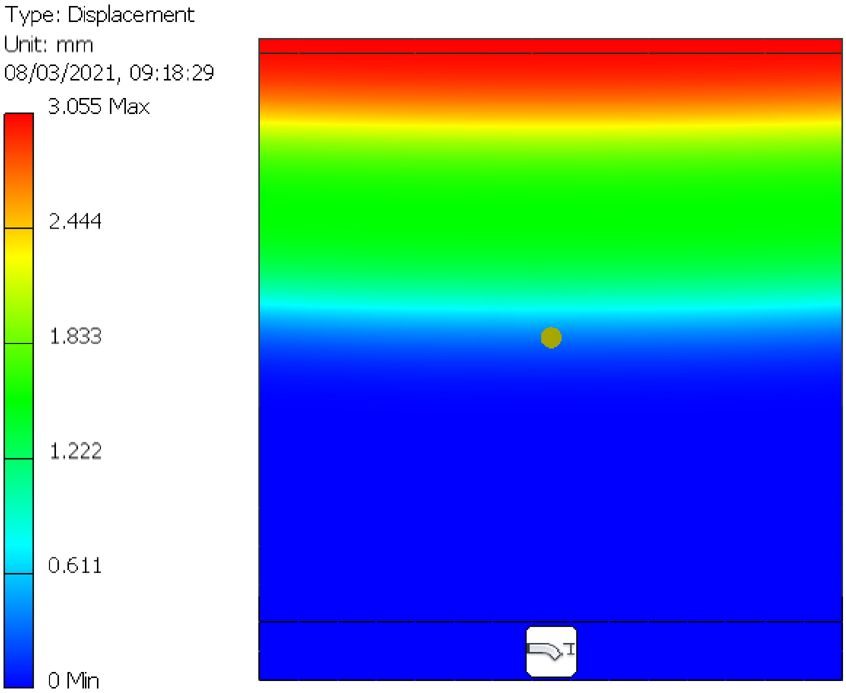
Glass Analysis - Deflection of Glass Panel due to 0.5kN Point Load:

- Analysis Software was used to determine maximum deflection of the glass due to 0.5kN Point Load
- 15mm Toughened Glass
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 3.055mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 19
Date: 11/03/2021	By: C.K. & R.F.

Glass Analysis – 17.52mm – EVA Interlayer:

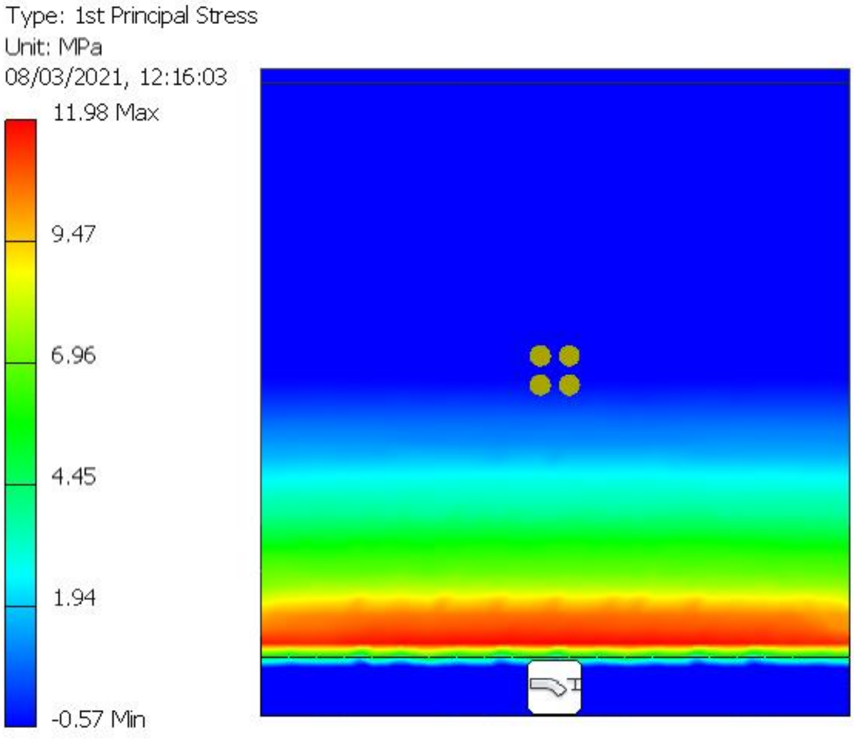
Glass Analysis - Bending Stress of Glass Panel due to 1.0kN/m2 Infill Loading:

- Analysis Software was used to determine maximum bending stress of the glass due to 1.0N/m2 Infill Loading
- 8/8/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 11.98N/mm^2 X 1.5 = 17.97N/mm^2 < 84.2N/mm^2

OK in Bending



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 20
Date: 11/03/2021	By: C.K. & R.F.

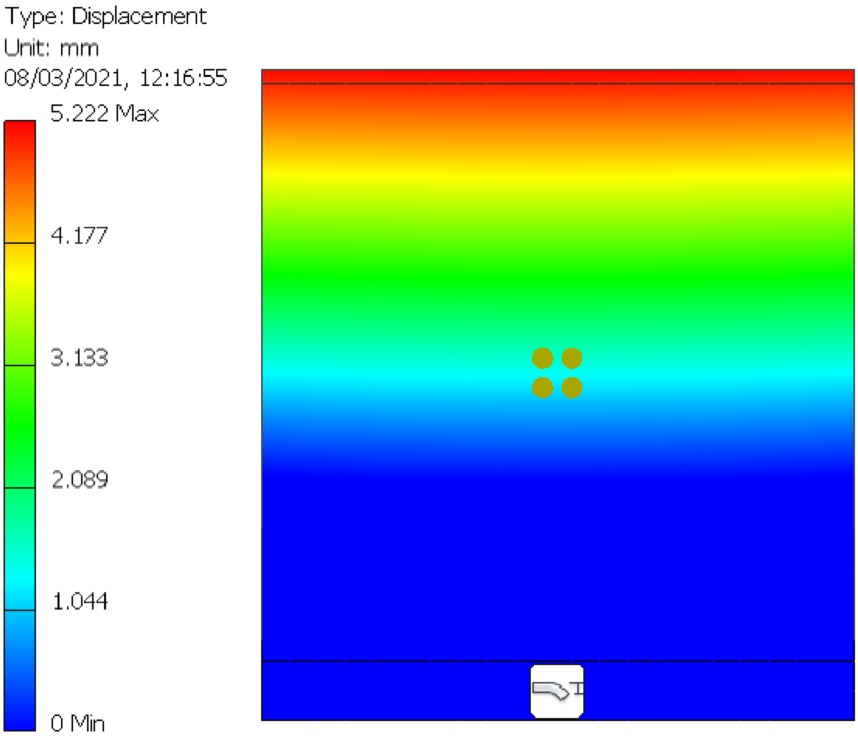
Glass Analysis - Deflection of Glass Panel due to 1.0kN/m2 Infill Loading:

- Analysis Software was used to determine maximum deflection of the glass due to 1.0N/m2 Infill Loading
- 8/8/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 5.222mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



TSA TED SINGLETON & ASSOCIATES CONSULTING ENGINEERS	**Project:** Concorde Glass Ltd.	**Contract:** 1507-1
	Subject: Glassloc Fixing & Wind Load Data	**Sheet No.** 21
	Date: 11/03/2021	**By:** C.K. & R.F.

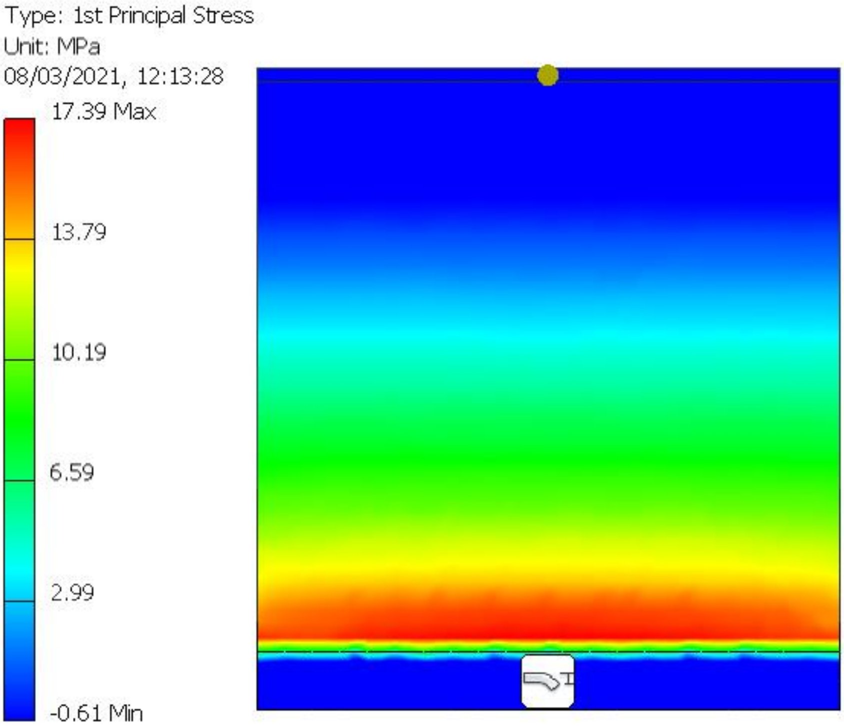
Glass Analysis - Bending Stress of Glass Panel due to 0.74kN/m Balustrade Loading:

- Analysis Software was used to determine maximum bending stress of the glass due to 0.74kN/m Balustrade Loading
- 8/8/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 17.39N/mm^2 X 1.5 = 26.085N/mm^2 < 84.2N/mm^2

OK in Bending



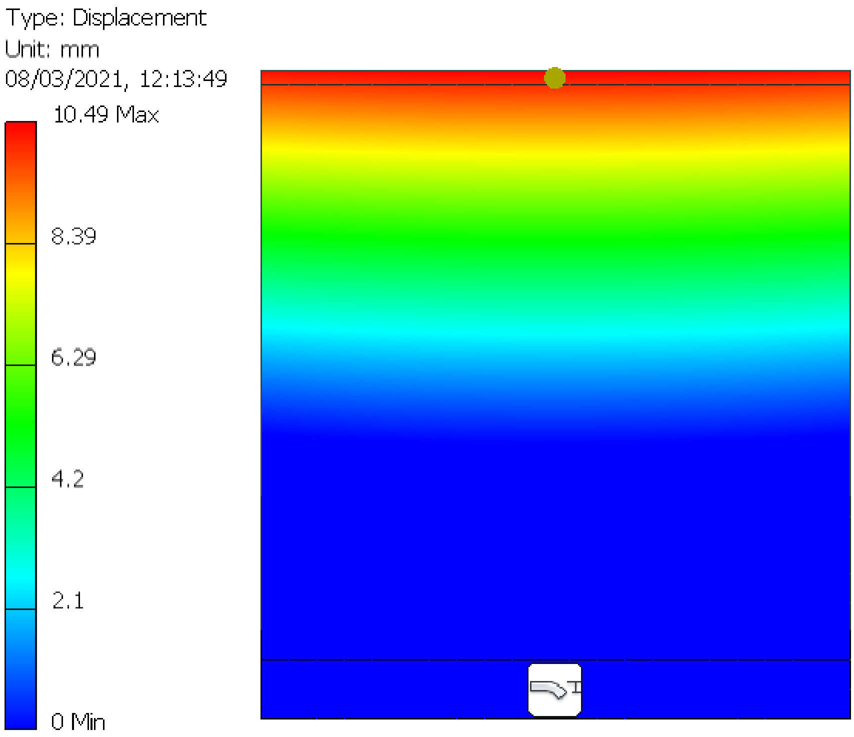
Glass Analysis - Deflection of Glass Panel due to 0.74kN/m Balustrade Loading:

- Analysis Software was used to determine maximum deflection of the glass due to 0.74kN/m Balustrade Loading
- 8/8/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 10.49mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



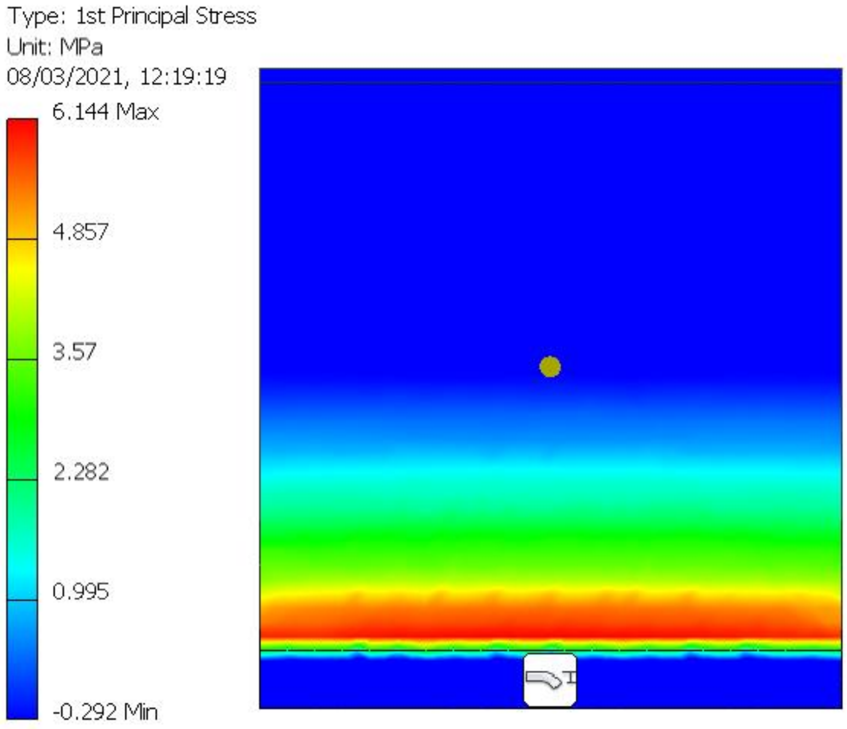
Glass Analysis - Bending Stress of Glass Panel due to 0.5kN Point Load:

- Analysis Software was used to determine maximum bending stress of the glass due to 0.5kN Point Load
- 8/8/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 6.144N/mm^2 X 1.5 = 9.216N/mm^2 < 84.2N/mm^2

OK in Bending



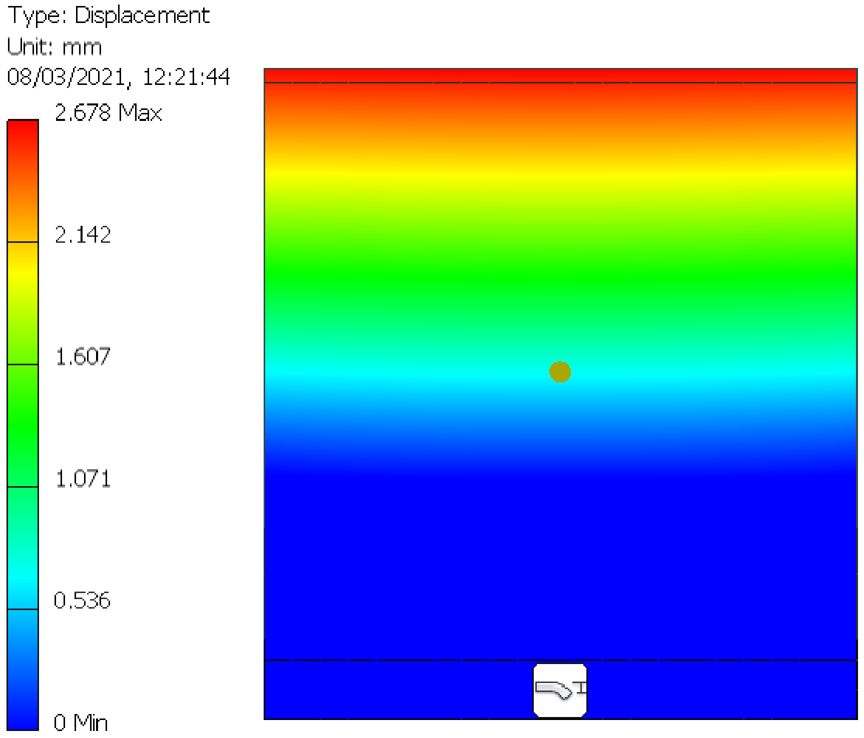
Glass Analysis - Deflection of Glass Panel due to 0.5kN Point Load:

- Analysis Software was used to determine maximum deflection of the glass due to 0.5kN Point Load
- 8/8/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 2.678mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



Project: Concorde Glass Ltd.	**Contract:** 1507-1
Subject: Glassloc Fixing & Wind Load Data	**Sheet No.** 25
Date: 11/03/2021	**By:** C.K. & R.F.

Glass Analysis – 21.52mm – EVA Interlayer:

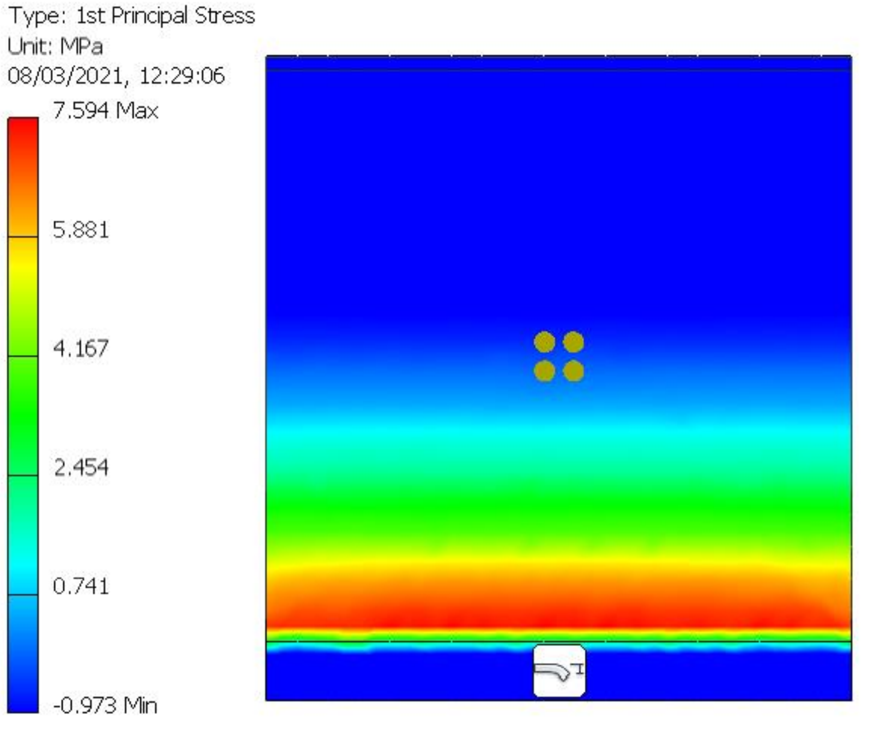
Glass Analysis - Bending Stress of Glass Panel due to 1.0kN/m2 Infill Loading:

- Analysis Software was used to determine maximum bending stress of the glass due to 1.0N/m2 Infill Loading
- 10/10/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 7.594N/mm^2 X 1.5 = 11.391N/mm^2 < 84.2N/mm^2

OK in Bending



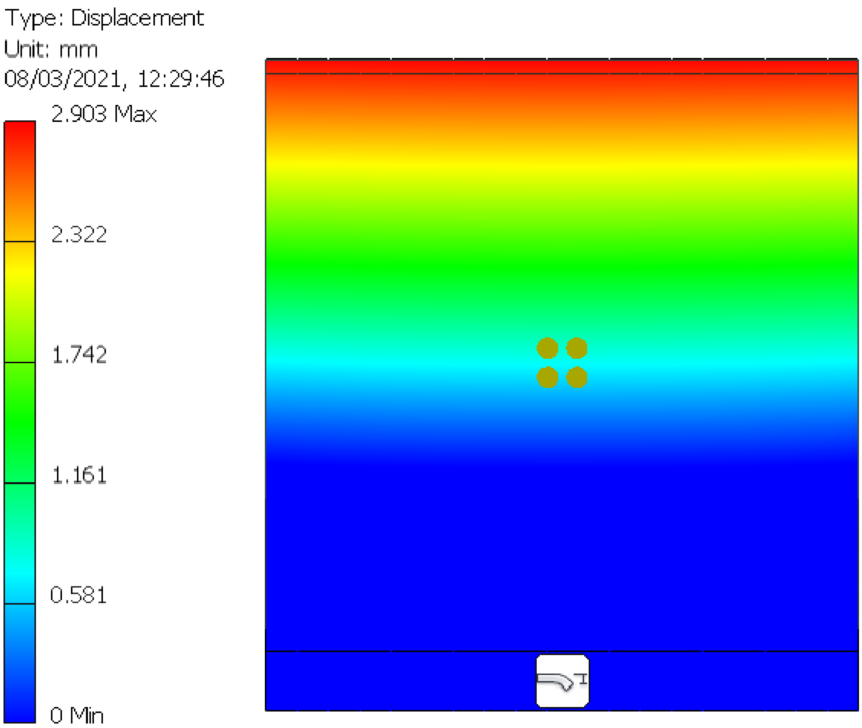
Glass Analysis - Deflection of Glass Panel due to 1.0kN/m2 Infill Loading:

- Analysis Software was used to determine maximum deflection of the glass due to 1.0N/m2 Infill Loading
- 10/10/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 2.903mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 27
Date: 11/03/2021	By: C.K. & R.F.

TSA
TED SINGLETON & ASSOCIATES
CONSULTING ENGINEERS

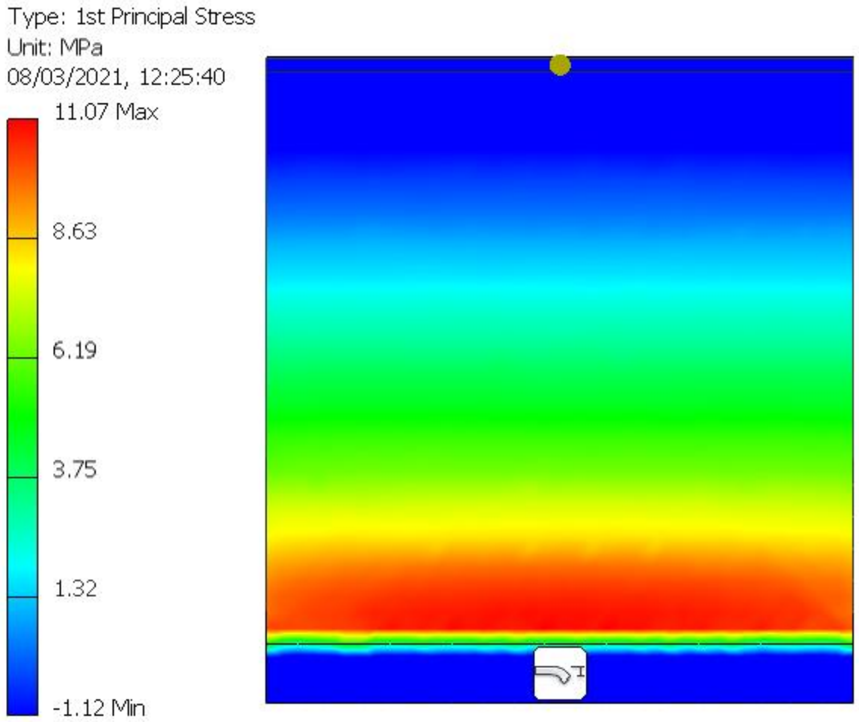
Glass Analysis - Bending Stress of Glass Panel due to 0.74kN/m Balustrade Loading:

- Analysis Software was used to determine maximum bending stress of the glass due to 0.74kN/m Balustrade Loading
- 10/10/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 11.07N/mm^2 X 1.5 = 16.605N/mm^2 < 84.2N/mm^2

OK in Bending



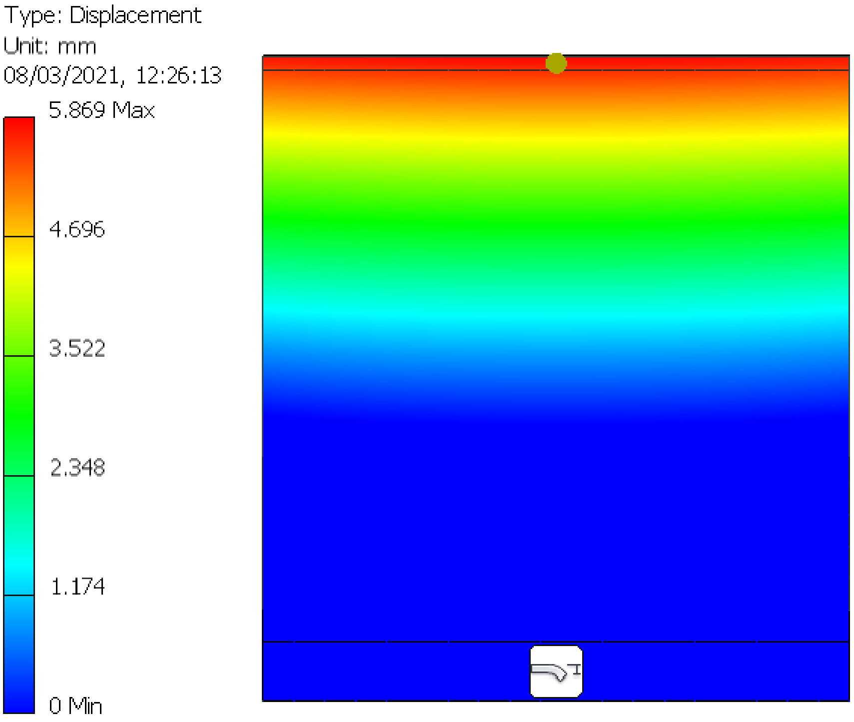
Glass Analysis - Deflection of Glass Panel due to 0.74kN/m Balustrade Loading:

- Analysis Software was used to determine maximum deflection of the glass due to 0.74kN/m Balustrade Loading
- 10/10/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 5.869mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



TSA TED SINGLETON & ASSOCIATES CONSULTING ENGINEERS	

Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 29
Date: 11/03/2021	By: C.K. & R.F.

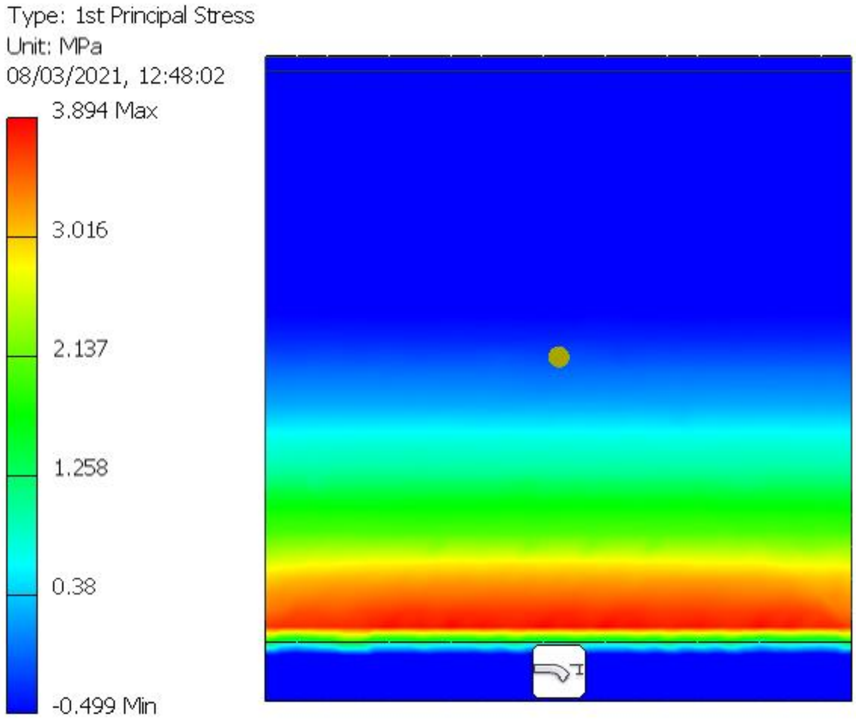
Glass Analysis - Bending Stress of Glass Panel due to 0.5kN Point Load:

- Analysis Software was used to determine maximum bending stress of the glass due to 0.5kN Point Load
- 10/10/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Bending Stress analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Bending Stress = 3.894N/mm^2 X 1.5 = 5.841N/mm^2 < 84.2N/mm^2

OK in Bending



TSA TED SINGLETON & ASSOCIATES CONSULTING ENGINEERS	**Project:** Concorde Glass Ltd.	**Contract:** 1507-1
	Subject: Glassloc Fixing & Wind Load Data	**Sheet No.** 30
	Date: 11/03/2021	**By:** C.K. & R.F.

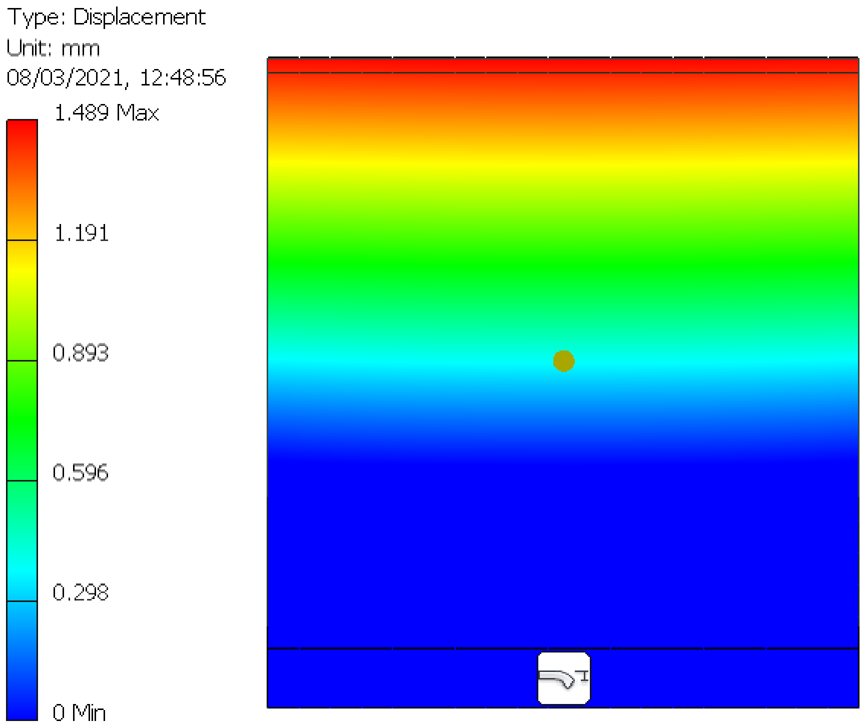
Glass Analysis - Deflection of Glass Panel due to 0.5kN Point Load:

- Analysis Software was used to determine maximum deflection of the glass due to 0.5kN Point Load
- 10/10/1.52mm T/L/T Glass analysed, horizontally toughened Laminated
- Interlayer Properties used for analysis, E= 18MPa, G = 6.82MPa EVA
- Deflection analysed based on glass panel of 1000 (l) x 1100 (h) mm

Result:

Max. Deflection = 1.489mm < 25mm {BS6180:2011 cl. 6.4.1}

OK in Deflection (Glass Only)



Shoe Analysis – Shoe – Balustrade Load 0.36kN/m:

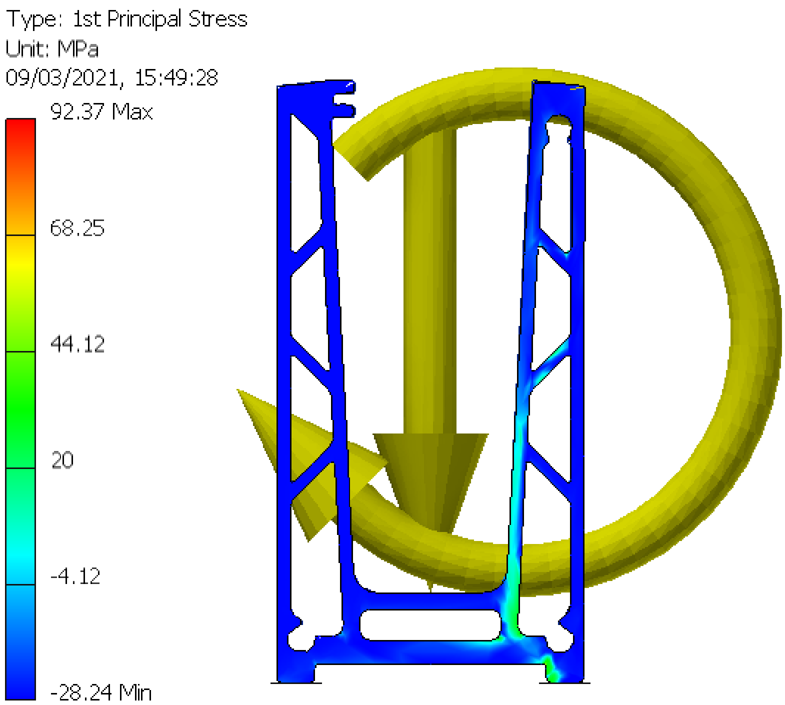
Bending Stress:

- Analysis Software was used to determine maximum bending stress of the shoe due to maximum Moment
- $\text{Moment} = 1.0\text{kN/m2} \times 1.0\text{m} \times 1.10\text{m} \times \frac{1.10\text{m}}{2} = 0.61\text{kN m(SLS)}$
- $\text{Weight (12mm)} = 287.76\text{N (SLS)}$

Result:

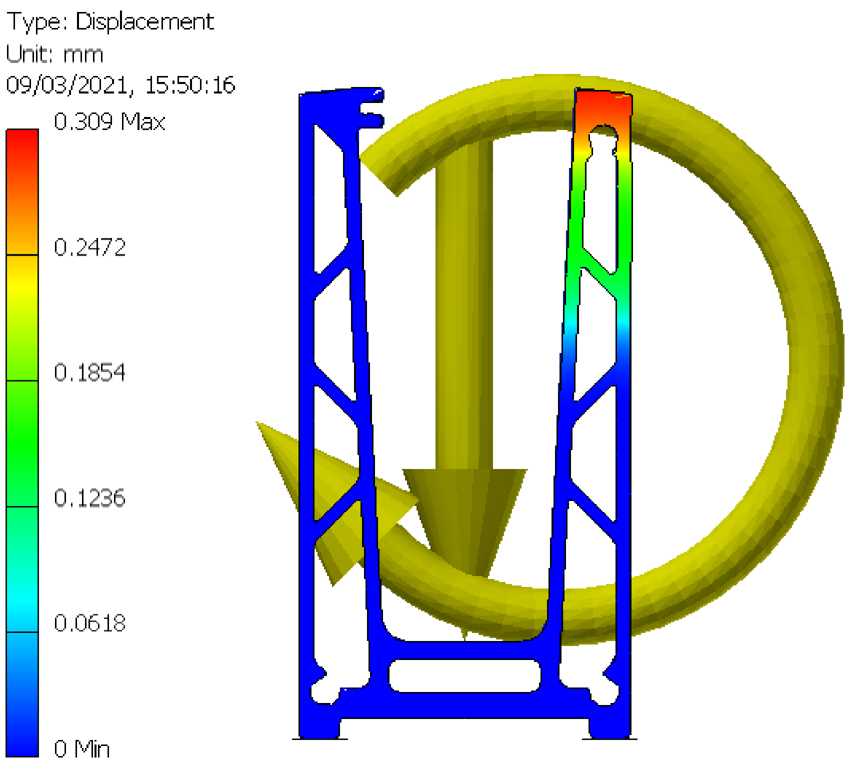
Max. Bending Stress = 92.37N/mm^2 x1.5 = 138.555N/mm^2 < 180N/mm^2

Okay in Bending



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 32
Date: 11/03/2021	By: C.K. & R.F.

Deflection:



NOTE:

- Deflection 0.309mm at the top of shoe
- Max. Deflection at 900mm above pitch line = (0.309 x 1100)/91 = 3.74mm

Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 33
Date: 11/03/2021	By: C.K. & R.F.

Shoe Analysis – Shoe – Balustrade Load 0.74kN/m:

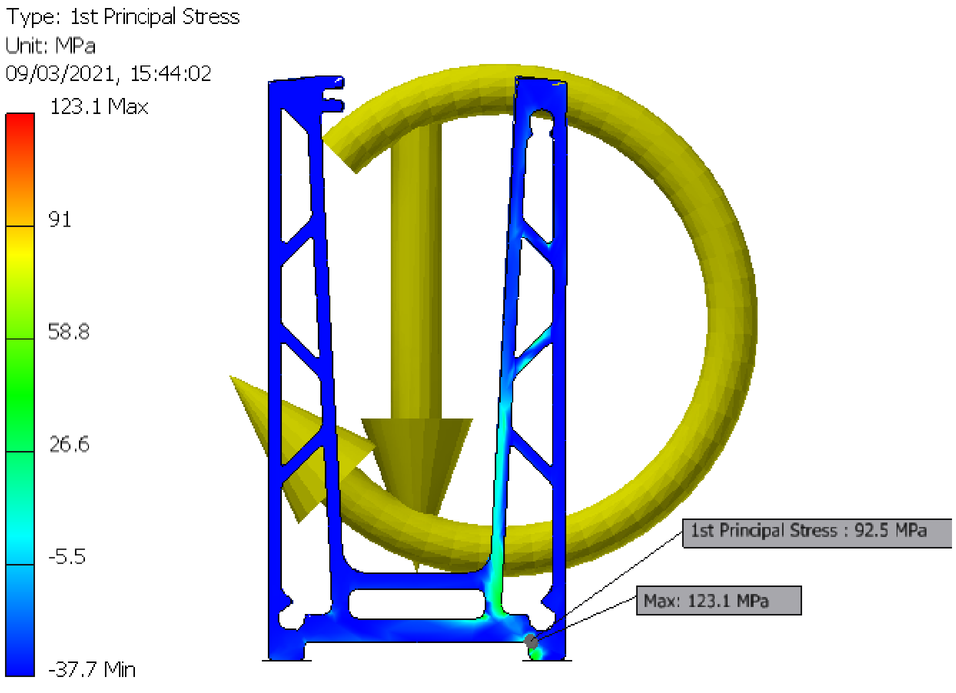
Bending Stress:

- Analysis Software was used to determine maximum bending stress of the shoe due to maximum Moment
- $\text{Moment} = 0.74\text{kN/m} \times 1.0\text{m} \times 1.10\text{m} = 0.814\text{kN m(SLS)}$
- $\text{Weight (21.52mm)} = 495.48\text{N (SLS)}$

Result:

Max. Bending Stress = 92.5N/mm^2 x1.5 = 138.75N/mm^2 < 180N/mm^2

Okay in Bending

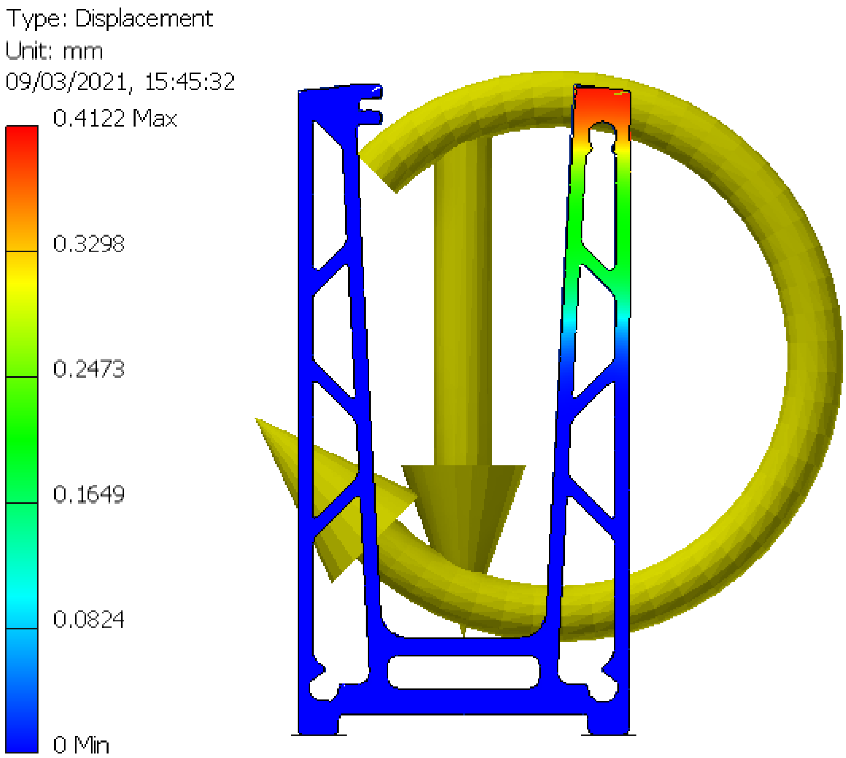


NOTE:

In this case the 123.1 MPa is a localised stress. The most appropriate stress to be considered is 92.5 MPa.

TSA TED SINGLETON & ASSOCIATES CONSULTING ENGINEERS	Project: Concorde Glass Ltd.	Contract: 1507-1
	Subject: Glassloc Fixing & Wind Load Data	Sheet No. 34
	Date: 11/03/2021	By: C.K. & R.F.

Deflection:



NOTE:

- Deflection 0.4122mm at the top of shoe
- Max. Deflection at 900mm above pitch line = (0.4122 x 1100)/91 = 4.98mm

Connection Design:

Case Study 01: 12mm Toughened Glass – 1.0x1.100m – 1.0kN/m^2

Case Study 02: 15mm Toughened Glass – 1.0x1.100m – 1.0kN/m^2

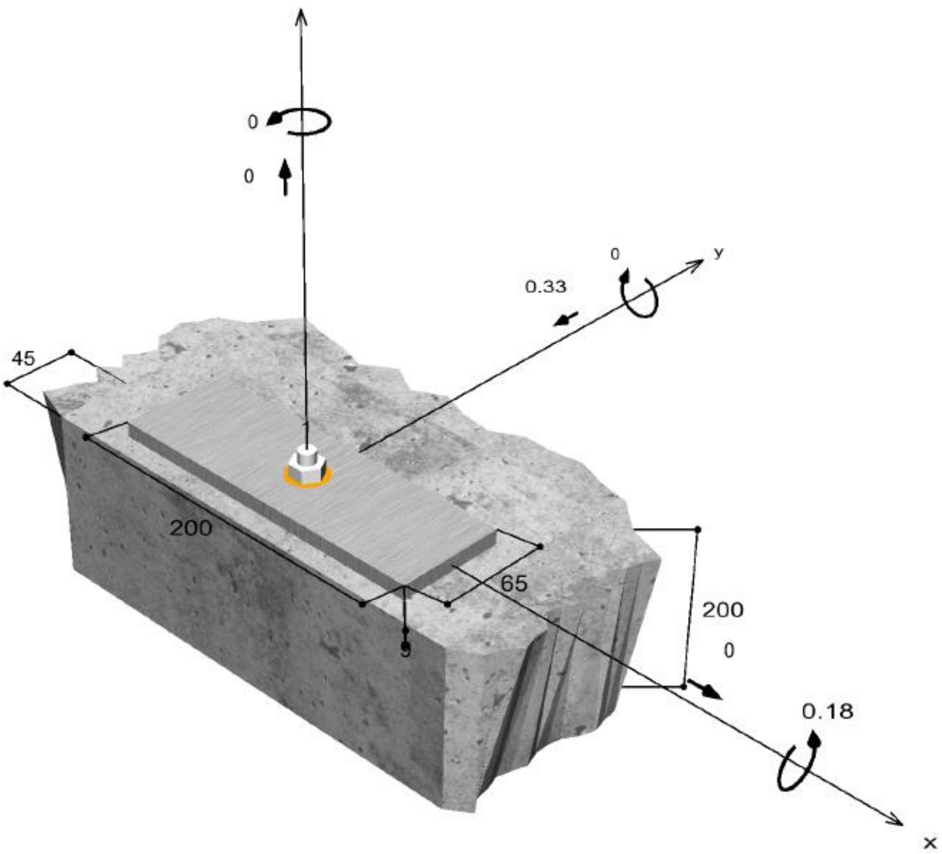
Case Study 03: 17.52mm Laminated Toughened Glass – 1.0x1.100m – 1.0kN/m^2

Case Study 04: 21.52mm Laminated Toughened Glass – 1.0x1.100m – 1.0kN/m^2

Connection to Concrete – Top Mounted Shoe

$$\text{Shear Load} = 1.0\text{kN/m}^2 \times 0.2\text{m} \times 1.100\text{m} \times 1.5 = 0.33\text{kN (ULS)}$$

$$\text{Moment} = 0.33\text{kN} \times (1.100\text{m} / 2) = 0.18\text{kNm (ULS)}$$



Therefore, use 1 Nr Anchor FIS V 360 S M10 x 110 @ 200mm c/c.

See design in Appendix B.

Connection to Mild Steel – Top Mounted Shoe:

1Nr M12 Bolt Grade 8.8

$f_y = 640\ MPa$ *(Grade 8.8 Mild Steel, Table 3.1 EN 1993-1-8:2005)*

$f_{ub} = 800\ MPa$ *(Grade 8.8 Mild Steel, Table 3.1 EN 1993-1-8:2005)*

$\alpha = 0.6$ *(Table 3.4 EN 1993-1-8:2005)*

$A = 84.3mm^2$ *(For M12 Bolts)*

$K_2 = 0.9$ *(Table 3.4 EN 1993-1-8:2005)*

$\lambda_{m2} = 1.25$ *(Table 5.1 EN 1993-1-4:2006)*

Tensile Resistance Check: *(Table 3.4 EN 1993-1-8:2005)*

$F_{t,Ed}$: *is the design tensile force per bolt for the ultimate limit state.*

$F_{t,Rd}$: *is the design tension resistance per bolt.*

$$\mathrm{F_{t,Ed}} = \frac{0.74kN/m \times 1.5 \times 1.100\mathrm{m} \times 0.6}{0.0325} = 22.54\mathrm{kN}$$

$$\mathrm{F_{t,Rd}} = \frac{\mathrm{K_2 F_{ub} A}}{\lambda \mathrm{m2}} \rightarrow \mathrm{F_{t,Rd}} = \frac{0.9 \times 800 \times 84.3 \times 10^{-3}}{1.25} = 48.5\mathrm{kN} > 22.54\mathrm{kN}$$ **Okay**

Shear Resistance Check: *(Table 3.4 EN 1993-1-8:2005)*

$F_{v,Ed}$: *is the design shear force per bolt for the ultimate limit state.*

$F_{v,Rd}$: *is the design shear resistance per bolt.*

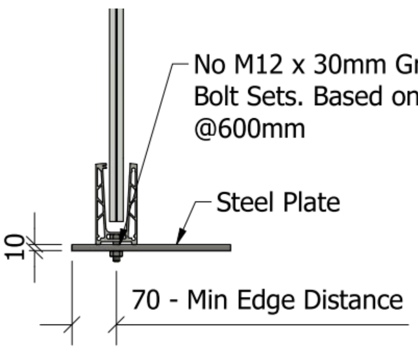
$$\mathrm{F_{V,Ed}} = 0.74\mathrm{kN/m} \times 1.5 \times 0.6 = 0.666\mathrm{kN}$$

$$\mathrm{F_{V,Rd}} = \frac{\alpha \mathrm{F_{ub} A}}{\lambda \mathrm{m2}} \rightarrow \mathrm{F_{V,Rd}} = \frac{0.6 \times 84.3 \times 800 \times 10^{-3}}{1.25} = 32.3\mathrm{kN} > 0.666\mathrm{kN}$$ **Okay**

Combined Shear & Tensile Resistance Check: *(Table 3.4 EN 1993-1-8:2005)*

$$\frac{F_{v,Ed}}{F_{v,Rd}} + \frac{F_{t,Ed}}{1.4F_{t,Rd}} \leq 1 \rightarrow \frac{0.666}{32.3} + \frac{22.54}{1.4 \times 48.5} = 0.35 \leq 1$$ **Okay**

Therefore, use 1Nr M12 Grade 8.8 Bolts at 600mm c/c.



Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 37
Date: 11/03/2021	By: C.K. & R.F.

Connection To Wood:

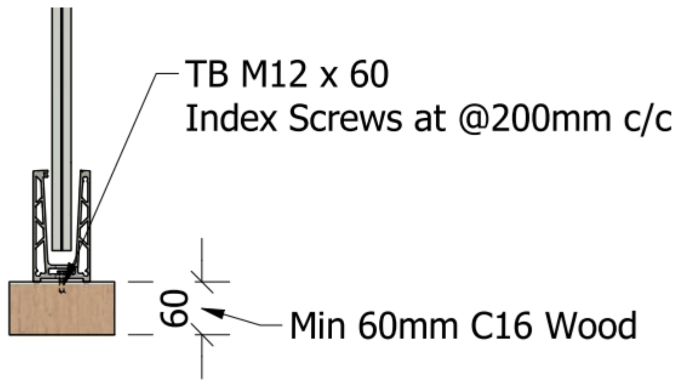
Tensile Resistance Check:

$$\text{Tensile Force per screw} = \frac{0.74kN/m \times 1.5 \times 1.100\text{m} \times 0.2}{0.0325} = 7.51\text{kN}$$

$\text{Tension Capacity of } 12 \times 60\text{mm Solo Screws} = 20.15\text{kN}$ as per specification sheet in appendix A.

$\text{Therefore}, 20.15\text{kN} > 5.58\text{kN}$ **Okay**

Therefore, use 1Nr TB M12×60 Index Screws at 200mm c/c or similar.



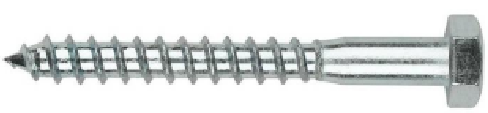
Project: Concorde Glass Ltd.	Contract: 1507-1
Subject: Glassloc Fixing & Wind Load Data	Sheet No. 38
Date: 11/03/2021	By: C.K. & R.F.

TSA
TED SINGLETON & ASSOCIATES
CONSULTING ENGINEERS

Appendix A –Index Wood Screws Specfication Sheet

2. INSTALLATION DATA

2.1 TB COACH SCREW DIN-571



Properties

Steel | Zinc coating | Self-tapping C tip

Main use

WOOD

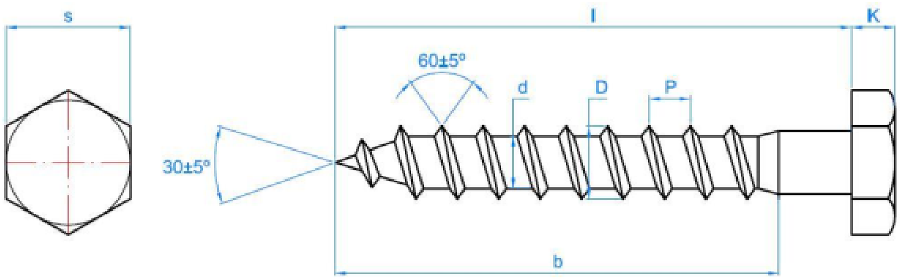
Properties

Installation with drill /screwdriver | Hexagonal

Characteristics and advantages

- Zinc coating
- Hexagonal head
- 60º thread
- C tip
- Application: Ironworks previously drilled to wood (Apt use with nylon plug)

Code		TB05	TB06	TB07	TB08	TB10	TB12	TB14
s: Head diameter	[mm]	8	10	12	13	17	19	22
D: Outer thread diameter	[mm]	5	6	7	8	10	12	14
d: Inner thread diameter	[mm]	3.5	4.2	4.9	5.6	7.0	9.0	10.5
p: Pitch	[mm]	2.2	2.6	3.2	3.5	4.5	5.0	5.5
k: Head thickness	[mm]	3.5	4.0	5.0	5.5	7.0	8.0	9.0
l: Screw length	[mm]	30 - 60	25 – 120	30 - 120	30 – 200	40 – 200	60 - 260	100
Hexagon dopbit code	[-]	BOCA008	BOCA010	---	---	---	---	---



TECHNICAL DATA SHEET

INDEX
A PERFECT FIXING

TECHNICAL CHARACTERISTICS									
Essential characteristics	Version	Performance							
		Unit	Ø 5	Ø 6	Ø 7	Ø 8	Ø 10	Ø 12	Ø 14
Characteristic yield moment $M_{y,k}$	Zinc	[mm]	30-60	25-120	30-120	30-200	40-200	60-260	100
Characteristic withdrawal parameter (along fibre) fax,k with ρ_k = 450 kg/m³	Zinc	[Nmm]	5984	10749	18047	24131	49056	81096	129198
Characteristic withdrawal parameter (across fibre) fax,k with ρ_k = 450 kg/m³	Zinc	[N/mm²]	14,20	14,74	14,36	13,38	10,58	11,92	10,86
Characteristic head pull-through parameter $f_{head,k}$ with ρ_k = 450 kg/m³	Zinc	[N/mm²]	9,31	7,73	10,33	6,72	6,71	7,62	7,05
Characteristic traction capacity $f_{tens,k}$	Zinc	[N/mm²]	26,42	24,90	24,74	22,55	21,37	20,15	20,23
Characteristic torsion ratio with ρ_k = 450 kg/m³	Zinc	[kN]	5,20	7,40	9,10	11,80	18,90	34,20	45,20
Corrosion protection	Zinc	[--]	3,47	2,44	2,88	2,45	3,07*	3,56*	3,49*
Characteristic yield moment $M_{y,k}$	Zinc	[--]	Service class 2 according to EN 1995-1-1						

(*) Predrilled
Coordinated technical specification: EN 14592:2008 + A1:2012

Appendix B - Fischer Reports

TSA is Both the Designer and the Specifier of the Fixings.

MASONRY FIXINGS

Unit 83, Cherry Orchard Industrial Estate
Dublin 10
Phone: +353 1 642 6700
Fax: +353 1 626 2197
technical@masonryfixings.ie
www.masonryfixings.ie

Design Specifications

Anchor

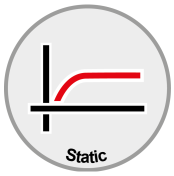
Anchor system	fischer Injection system FIS V
Injection resin	FIS V 360 S
Fixing element	Threaded rod FIS A M 10 x 110, zinc plated steel, Property Class 5.8
Calculated anchorage depth	60 mm
Design Data	Anchor design in Concrete according European Technical Assessment ETA-02/0024, Option 1, Issued 13/05/2020

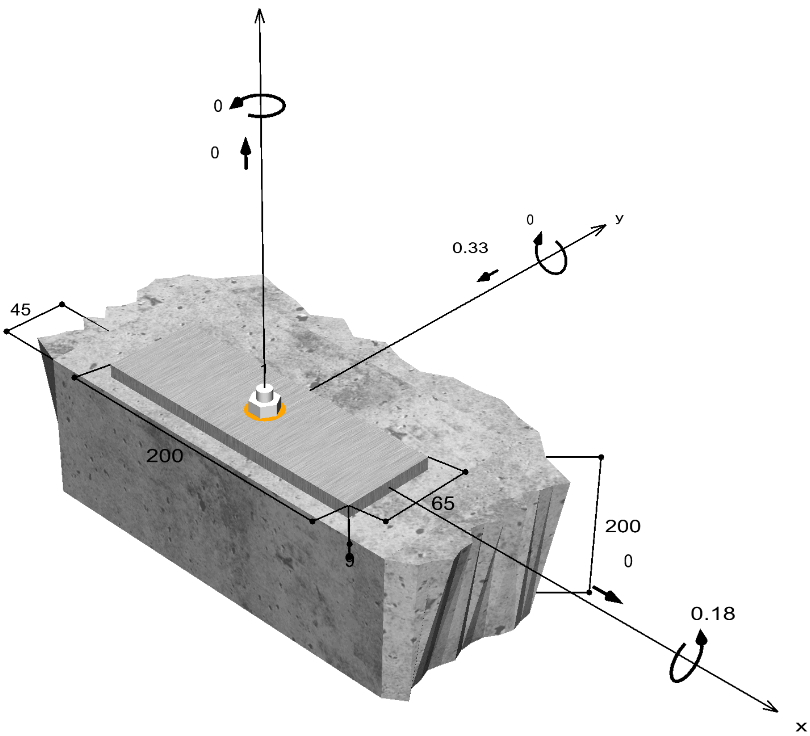
Geometry / Loads / Scale units

mm, kN, kNm

Value of design actions (including

partial safety factor for the load)





Not drawn to scale

Input data

Design method	Design Method EN1992-4:2018 bonded fastener
Base material	C30/37, EN 206
Concrete condition	Non-cracked, dry hole
Temperature range	24 °C long term temperature, 40 °C short term temperature
Reinforcement	Normal or no reinforcement. No edge reinforcement
Drilling method	Hammer drilling
Installation type	Push-through installation
Annular gap	Annular gap filled
Type of loading	Permanent-Transient/Static
Base plate location	Base plate flush installed on base material
Base plate geometry	200 mm x 65 mm x 9 mm
Profile type	None

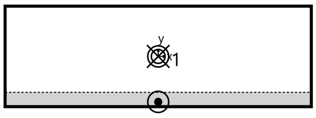
Design actions *)

#	N_{Ed} kN	$V_{Ed,x}$ kN	$V_{Ed,y}$ kN	$M_{Ed,x}$ kNm	$M_{Ed,y}$ kNm	$M_{T,Ed}$ kNm	Type of loading
1	0.00	0.00	-0.33	0.18	0.00	0.00	Permanent-Transient/Static

*) The required partial safety factors for actions are included

Resulting anchor forces

Anchor no.	Tensile action kN	Shear Action kN	Shear Action x kN	Shear Action y kN
1	6.12	0.33	0.00	-0.33



max. concrete compressive strain :	0.20 ‰
max. concrete compressive stress :	6.6 N/mm²
Resulting tensile actions :	6.12 kN , X/Y position (0 / 0)
Resulting compression actions :	6.12 kN , X/Y position (0 / -29)

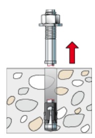
Resistance to tension loads

Proof	Action kN	Capacity kN	Utilisation β_N %
Steel failure *	6.12	19.33	31.7
Combined pull-out and concrete cone failure	6.12	9.69	**63.1**
Concrete cone failure	6.12	11.90	51.4
Splitting failure	6.12	14.47	42.3

* Most unfavourable anchor

Steel failure

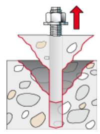
$$N_{Ed} \leq \frac{N_{Rk,s}}{\gamma_{Ms}}$$ **($N_{Rd,s}$)**



$N_{Rk,s}$ kN	γ_{Ms}	$N_{Rd,s}$ kN	N_{Ed} kN	$\beta_{N,s}$ %
29.00	1.50	19.33	6.12	31.7

Anchor no.	$\beta_{N,s}$ %	Group N°	Decisive Beta
1	31.7	1	$\beta_{N,s;1}$

Combined pull-out and concrete cone failure



$$N_{Ed} \leq \frac{N_{Rk,p}}{\gamma_{Mp}} \quad (N_{Rd,p})$$

$$N_{Rk,p} = N^0_{Rk,p} \cdot \frac{A_{p,N}}{A^0_{p,N}} \cdot \Psi_{s,Np} \cdot \Psi_{g,Np} \cdot \Psi_{ec,Np} \cdot \Psi_{re,Np}$$ Eq. (7.13)

$$N_{Rk,p} = 22.81kN \cdot \frac{24{,}300mm^2}{32{,}400mm^2} \cdot 0.850 \cdot 1.000 \cdot 1.000 \cdot 1.000 = 14.54kN$$

$$N^0_{Rk,p} = \Psi_{sus} \cdot \pi \cdot d \cdot h_{ef} \cdot \tau_{Rk} = 1.00 \cdot \pi \cdot 10mm \cdot 60mm \cdot 12.1N/mm^2 = 22.81kN$$ Eq. (7.14)

$$\Psi_{sus} = 1.00$$ Eq. (7.14a)

$$\alpha_{sus} = 0.00 \leq \Psi^0_{sus} = 0.74$$

$$s_{cr,Np} = min\left(7.3 \cdot d \cdot \left(\Psi_{sus} \cdot \tau_{Rk,ucr}\right)^{0.5}; 3 \cdot h_{ef}\right)$$ Eq. (7.15)

$$s_{cr,Np} = min\left(7.3 \cdot 10mm \cdot \left(1.00 \cdot 11.0N/mm^2\right)^{0.5}; 3 \cdot 60mm\right) = 180mm$$

$$c_{cr,Np} = \frac{S_{cr,Np}}{2} = \frac{180mm}{2} = 90mm$$ Eq. (7.16)

$$\Psi_{s,Np} = 0.7 + 0.3 \cdot \frac{c}{c_{cr,Np}} = 0.7 + 0.3 \cdot \frac{45mm}{90mm} = 0.850 \leq 1$$ Eq. (7.20)

$$\Psi_{g,Np} = max\left(1; \Psi^0_{g,Np} - \sqrt{\frac{s}{s_{cr,Np}}} \cdot \left(\Psi^0_{g,Np} - 1\right)\right) = 1.000 - \sqrt{\frac{0mm}{180mm}} \cdot \left(1.000 - 1\right) = 1.000 \geq 1$$ Eq. (7.17)

$$\Psi^0_{g,Np} = max\left(1; \sqrt{n} - \left(\sqrt{n} - 1\right) \cdot \left(\frac{\tau_{Rk}}{\tau_{Rk,c}}\right)^{1.5}\right)$$ Eq. (7.18)

$$\Psi^0_{g,Np} = max\left(1; \sqrt{1} - \left(\sqrt{1} - 1\right) \cdot \left(\frac{12.1N/mm^2}{14.9N/mm^2}\right)^{1.5}\right) = 1.000 \geq 1$$

$$\tau_{Rk,c} = \frac{k_3}{\pi \cdot d}\sqrt{h_{ef} \cdot f_{ck}} = \frac{11}{3.14 \cdot 10mm}\sqrt{60mm \cdot 30.0N/mm^2} = 14.9N/mm^2$$ Eq. (7.19)

$$\Psi_{ec,Np} = \frac{1}{1 + \frac{2e_n}{s_{cr,Np}}} = \Psi_{ec,Npx} \cdot \Psi_{ec,Npy} = 1.000 \cdot 1.000 = 1.000 \leq 1$$ Eq. (7.21)

$$\Psi_{ec,Npx} = \frac{1}{1 + \frac{2 \cdot 0mm}{180mm}} = 1.000 \leq 1 \qquad \Psi_{ec,Npy} = \frac{1}{1 + \frac{2 \cdot 0mm}{180mm}} = 1.000 \leq 1$$

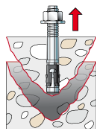
$$\Psi_{re,Np} = 1.000$$ Eq. (7.5)

$N_{Rk,p}$ kN	γ_{Mp}	$N_{Rd,p}$ kN	N_{Ed} kN	$\beta_{N,p}$ %
14.54	1.50	9.69	6.12	63.1

Anchor no.	$\beta_{N,p}$ %	Group N°	Decisive Beta
1	63.1	1	$\beta_{N,p;1}$

Concrete cone failure

$$N_{Ed} \leq \frac{N_{Rk,c}}{\gamma_{Mc}} \quad (\mathbf{N_{Rd,c}})$$



$$N_{Rk,c} = N^0_{Rk,c} \cdot \frac{A_{c,N}}{A^0_{c,N}} \cdot \Psi_{s,N} \cdot \Psi_{re,N} \cdot \Psi_{ec,N} \cdot \Psi_{M,N}$$ Eq. (7.1)

$$N_{Rk,c} = 28.00kN \cdot \frac{24{,}300mm^2}{32{,}400mm^2} \cdot 0.850 \cdot 1.000 \cdot 1.000 \cdot 1.000 = 17.85kN$$

$$N^0_{Rk,c} = k_1 \cdot \sqrt{f_{ck}} \cdot h_{ef}^{1.5} = 11.0 \cdot \sqrt{30.0N/mm^2} \cdot \left(60mm\right)^{1.5} = 28.00kN$$ Eq. (7.2)

$$\Psi_{s,N} = 0.7 + 0.3 \cdot \frac{c}{c_{cr,N}} = 0.7 + 0.3 \cdot \frac{45mm}{90mm} = 0.850 \leq 1$$ Eq. (7.4)

$$\Psi_{re,N} = 1.000$$ Eq. (7.5)

$$\Psi_{ec,N} = \frac{1}{1 + \frac{2e_n}{s_{cr,N}}} \Longrightarrow \Psi_{ec,Nx} \cdot \Psi_{ec,Ny} = 1.000 \cdot 1.000 = 1.000 \leq 1$$ Eq. (7.6)

$$\Psi_{ec,Nx} = \frac{1}{1 + \frac{2 \cdot 0mm}{180mm}} = 1.000 \leq 1 \qquad \Psi_{ec,Ny} = \frac{1}{1 + \frac{2 \cdot 0mm}{180mm}} = 1.000 \leq 1$$

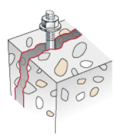
$$\Psi_{M,N} = 1.00 \geq 1$$ Eq. (7.7)

$N_{Rk,c}$ kN	γ_{Mc}	$N_{Rd,c}$ kN	N_{Ed} kN	$\beta_{N,c}$ %
17.85	1.50	11.90	6.12	51.4

Anchor no.	$\beta_{N,c}$ %	Group N°	Decisive Beta
1	51.4	1	$\beta_{N,c;1}$

Splitting failure due to loading

$$N_{Ed} \leq \frac{N_{Rk,sp}}{\gamma_{Msp}} \quad (\mathbf{N_{Rd,sp}})$$



$$N_{Rk,sp} = N^0_{Rk,sp} \cdot \frac{A_{c,N}}{A^0_{c,N}} \cdot \Psi_{s,N} \cdot \Psi_{re,N} \cdot \Psi_{ec,N} \cdot \Psi_{h,sp}$$ Eq. (7.23)

$$N_{Rk,sp} = 22.81kN \cdot \frac{12{,}600mm^2}{14{,}400mm^2} \cdot 0.925 \cdot 1.000 \cdot 1.000 \cdot 1.176 = 21.71kN$$

$$\Psi_{s,N} = 0.7 + 0.3 \cdot \frac{c}{c_{cr,sp}} = 0.7 + 0.3 \cdot \frac{45mm}{60mm} = 0.925 \leq 1$$ Eq. (7.4)

$$\Psi_{re,N} = 1.000$$ Eq. (7.5)

$$\Psi_{ec,N} = \frac{1}{1 + \frac{2e_n}{s_{cr,sp}}} = \Psi_{ec,Nx} \cdot \Psi_{ec,Ny} = 1.000 \cdot 1.000 = 1.000 \leq 1$$ Eq. (7.6)

$$\Psi_{ec,Nx} = \frac{1}{1 + \frac{2 \cdot 0mm}{120mm}} = 1.000 \leq 1 \qquad \Psi_{ec,Ny} = \frac{1}{1 + \frac{2 \cdot 0mm}{120mm}} = 1.000 \leq 1$$

$$\Psi_{h,sp} = min\left(\left(\frac{h}{h_{min}}\right)^{2/3} ;max\left(1; \left(\frac{h_{ef} + 1.5\ c_1}{h_{min}}\right)^{2/3}\right);2\right)$$ Eq. (7.24)

$$\Psi_{h,sp} = min\left(\left(\frac{200mm}{100mm}\right)^{2/3} ;max\left(1; \left(\frac{60mm + 1.5 \cdot 45mm}{100mm}\right)^{2/3}\right);2\right) = 1.176$$

$N_{Rk,sp}$ kN	γ_{Msp}	$N_{Rd,sp}$ kN	N_{Ed} kN	$\beta_{N,sp}$ %
21.71	1.50	14.47	6.12	42.3

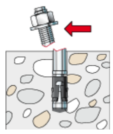
Anchor no.	$\beta_{N,sp}$ %	Group N°	Decisive Beta
1	42.3	1	$\beta_{N,sp;1}$

Resistance to shear loads

Proof	Action kN	Capacity kN	Utilisation β_V %
Steel failure without lever arm *	0.33	13.60	2.4
Concrete pry-out failure	0.33	19.39	1.7
Concrete edge failure	0.33	4.67	**7.1**

* Most unfavourable anchor

Steel failure without lever arm



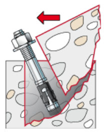
$$V_{Ed} \leq \frac{V_{Rk,s}}{\gamma_{Ms}}$$ **($V_{Rd,s}$)**

$$V_{Rk,s} = k_7 \cdot V^0_{Rk,s} = 1.00 \cdot 17.00kN = 17.00kN$$ Eq. (7.35)/ (7.36)

$V_{Rk,s}$ kN	γ_{Ms}	$V_{Rd,s}$ kN	V_{Ed} kN	β_{Vs} %
17.00	1.25	13.60	0.33	2.4

Anchor no.	β_{Vs} %	Group N°	Decisive Beta
1	2.4	1	$\beta_{Vs;1}$

Concrete pry-out failure



$$V_{Ed} \leq \frac{V_{Rk,cp}}{\gamma_{Mc}} \quad \textbf{(V}_{\textbf{Rd,cp}}\textbf{)}$$

$$V_{Rk,cp} = k_8 \cdot N_{Rk,p} = 2 \cdot 14.54kN = 29.08kN$$ Eq. (7.39c)

$$N_{Rk,p} = N^0_{Rk,p} \cdot \frac{A_{p,N}}{A^0_{p,N}} \cdot \Psi_{s,Np} \cdot \Psi_{g,Np} \cdot \Psi_{ec,Np} \cdot \Psi_{re,Np}$$ Eq. (7.13)

$$N_{Rk,p} = 22.81kN \cdot \frac{24{,}300mm^2}{32{,}400mm^2} \cdot 0.850 \cdot 1.000 \cdot 1.000 \cdot 1.000 = 14.54kN$$

$$N^0_{Rk,p} = \Psi_{sus} \cdot \pi \cdot d \cdot h_{ef} \cdot \tau_{Rk} = 1.00 \cdot \pi \cdot 10mm \cdot 60mm \cdot 12.1N/mm^2 = 22.81kN$$ Eq. (7.14)

$$\Psi_{sus} = 1.00$$ Eq. (7.14a)

$$\alpha_{sus} = 0.00 \leq \Psi^0_{sus} = 0.74$$

$$s_{cr,Np} = min\left(7.3 \cdot d \cdot \left(\Psi_{sus} \cdot \tau_{Rk,ucr}\right)^{0.5}; 3 \cdot h_{ef}\right)$$ Eq. (7.15)

$$s_{cr,Np} = min\left(7.3 \cdot 10mm \cdot \left(1.00 \cdot 11.0N/mm^2\right)^{0.5}; 3 \cdot 60mm\right) = 180mm$$

$$c_{cr,Np} = \frac{S_{cr,Np}}{2} = \frac{180mm}{2} = 90mm$$ Eq. (7.16)

$$\Psi_{s,Np} = 0.7 + 0.3 \cdot \frac{c}{c_{cr,Np}} = 0.7 + 0.3 \cdot \frac{45mm}{90mm} = 0.850 \leq 1$$ Eq. (7.20)

$$\Psi_{g,Np} = max\left(1; \Psi^0_{g,Np} - \sqrt{\frac{s}{s_{cr,Np}}} \cdot \left(\Psi^0_{g,Np} - 1\right)\right)$$ Eq. (7.17)

$$\Psi_{g,Np} = max\left(1; 1.000 - \sqrt{\frac{0mm}{180mm}} \cdot \left(1.000 - 1\right)\right) = 1.000 \geq 1$$

$$\Psi^0_{g,Np} = max\left(1; \sqrt{n} - \left(\sqrt{n} - 1\right) \cdot \left(\frac{\tau_{Rk}}{\tau_{Rk,c}}\right)^{1.5}\right)$$ Eq. (7.18)

$$\Psi^0_{g,Np} = max\left(1; \sqrt{1} - \left(\sqrt{1} - 1\right) \cdot \left(\frac{12.1N/mm^2}{14.9N/mm^2}\right)^{1.5}\right) = 1.000 \geq 1$$

$$\tau_{Rk,c} = \frac{k_3}{\pi \cdot d}\sqrt{h_{ef} \cdot f_{ck}} = \frac{11}{3.14 \cdot 10mm}\sqrt{60mm \cdot 30.0N/mm^2} = 14.9N/mm^2$$ Eq. (7.19)

$$\Psi_{ec,Np} = \frac{1}{1 + \frac{2e_n}{s_{cr,Np}}} = \Psi_{ec,Npx} \cdot \Psi_{ec,Npy} = 1.000 \cdot 1.000 = 1.000 \leq 1$$ Eq. (7.21)

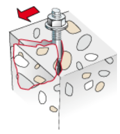
$$\Psi_{re,Np} = 1.000$$ Eq. (7.5)

$V_{Rk,cp}$ kN	γ_{Mcp}	$V_{Rd,cp}$ kN	V_{Ed} kN	$\beta_{V,cp}$ %
29.08	1.50	19.39	0.33	1.7

Anchor no.	$\beta_{V,cp}$ %	Group N°	Decisive Beta
1	1.7	1	$\beta_{V,cp;1}$

Concrete edge failure

$$V_{Ed} \leq \frac{V_{Rk,c}}{\gamma_{Mc}} \qquad (V_{Rd,c})$$



$$V_{Rk,c} = V^0_{Rk,c} \cdot \frac{A_{c,V}}{A^0_{c,V}} \cdot \Psi_{s,V} \cdot \Psi_{h,V} \cdot \Psi_{\alpha,V} \cdot \Psi_{ec,V} \cdot \Psi_{re,V} \qquad \text{Eq. (7.40)}$$

$$V_{Rk,c} = 7.01kN \cdot \frac{9{,}113mm^2}{9{,}113mm^2} \cdot 1.000 \cdot 1.000 \cdot 1.000 \cdot 1.000 \cdot 1.000 = 7.01kN$$

$$V^0_{Rk,c} = k_9 \cdot d^\alpha \cdot l_f^\beta \cdot \sqrt{f_{ck}} \cdot c_1^{1.5} \qquad \text{Eq. (7.41)}$$

$$V^0_{Rk,c} = 2.4 \cdot \left(10mm\right)^{0.115} \cdot \left(60mm\right)^{0.074} \cdot \sqrt{30.0N/mm^2} \cdot \left(45mm\right)^{1.5} = 7.01kN$$

$$\alpha = 0.1 \cdot \sqrt{\frac{l_f}{c_1}} = 0.1 \cdot \sqrt{\frac{60mm}{45mm}} = 0.115 \qquad \beta = 0.1 \cdot \left(\frac{d}{c_1}\right)^{0.2} = 0.1 \cdot \left(\frac{10mm}{45mm}\right)^{0.2} = 0.074 \qquad \text{Eq. (7.42/7.43)}$$

$$\Psi_{s,V} = 0.7 + 0.3 \cdot \frac{c_2}{1.5c_1} = 0.7 + 0.3 \cdot \frac{68mm}{1.5 \cdot 45mm} = 1.000 \leq 1 \qquad \text{Eq. (7.45)}$$

$$\Psi_{h,V} = max\left(1; \sqrt{\frac{1.5c_1}{h}}\right) = max\left(1; \sqrt{\frac{1.5 \cdot 45mm}{200mm}}\right) = 1.000 \geq 1 \qquad \text{Eq. (7.46)}$$

$$\Psi_{\alpha,V} = \sqrt{\frac{1}{\left(cos\ \alpha_V\right)^2 + \left(0.5 \cdot sin\ \alpha_V\right)^2}} = \sqrt{\frac{1}{\left(cos\ 0.0\right)^2 + \left(0.5 \cdot sin\ 0.0\right)^2}} = 1.000 \geq 1 \qquad \text{Eq. (7.48)}$$

$$\Psi_{ec,V} = \frac{1}{1 + \frac{2}{3}\frac{e_v}{c_1}} = \frac{1}{1 + \frac{2 \cdot 0mm}{3 \cdot 45mm}} = 1.000 \leq 1 \qquad \text{Eq. (7.47)}$$

$$\Psi_{re,V} = 1.000$$

$V_{Rk,c}$ kN	γ_{Mc}	$V_{Rd,c}$ kN	V_{Ed} kN	$\beta_{V,c}$ %
7.01	1.50	4.67	0.33	7.1

Anchor no.	$\beta_{V,c}$ %	Group N°	Decisive Beta
1	7.1	1	$\beta_{V,c;1}$

Utilization of tension and shear loads

Tension loads	Utilisation βN %
Steel failure *	31.7
Combined pull-out and concrete cone failure	**63.1**
Concrete cone failure	51.4
Splitting failure	42.3

Shear Loads	Utilisation βV %
Steel failure without lever arm *	2.4
Concrete pry-out failure	1.7
Concrete edge failure	**7.1**

* Most unfavourable anchor

Resistance to combined tensile and shear loads

Utilisation steel

$$\beta_{N.s} = \beta_{N,s;1} = 0.32 \leq 1$$
$$\beta_{V.s} = \beta_{Vs;1} = 0.02 \leq 1$$
$$\beta_N^2 + \beta_V^2 = \beta_{N,s;1}^2 + \beta_{Vs;1}^2 = 0.10 \leq 1$$ Eq. (7.55)

Utilisation concrete

Proof successful

$$\beta_{N,p} = \beta_{N,p;1} = 0.63 \leq 1$$
$$\beta_{V.c} = \beta_{V,c;1} = 0.07 \leq 1$$
$$\beta_N^{1.5} + \beta_V^{1.5} = \beta_{N,p;1}^{1.5} + \beta_{V,c;1}^{1.5} = 0.52 \leq 1$$ Eq. (7.56)

Information concerning the anchor plate

Base plate details

Plate thickness specified by user without proof t = 9 mm

Profile type None

Technical remarks

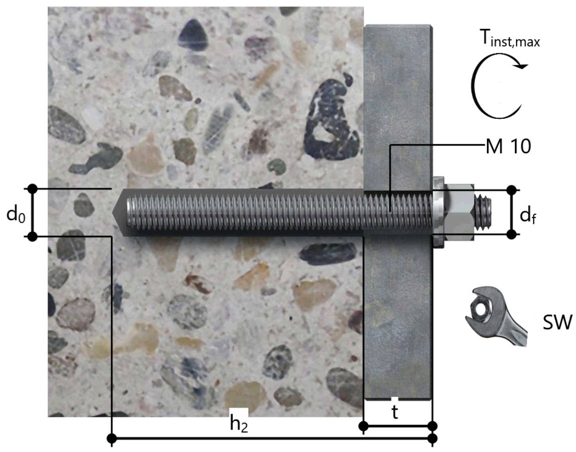
The transmission of the anchor loads to the supports of the concrete member shall be shown for the ultimate limit state and the serviceability limit state; for this purpose, the normal verifications shall be carried out under due consideration of the actions introduced by the anchors. For these verifications the additional provisions given in the current design method shall be taken into account.
As a pre-condition the anchor plate is assumed to be flat when subjected to the actions. Therefore, the plate (if present) must be sufficiently stiff. The C-Fix anchor plate design is based on a proof of stresses and does not allow a statement about the stiffness of the plate. The proof of the necessary stiffness is not carried out by C-Fix.

Installation data

Anchor

Anchor system	**fischer Injection system FIS V**	
Injection resin	FIS V 360 S (other cartridge sizes available)	Art.-No. 94405
Fixing element	Threaded rod FIS A M 10 x 110, zinc plated steel, Property Class 5.8	Art.-No. 90278
Accessories	FIS MR Plus	Art.-No. 545853
	Dispenser FIS DM S	Art.-No. 511118
	Blow-out pump ABG big	Art.-No. 89300
	Cleaning brush BS 12	Art.-No. 78179
	SDS Plus II 12/100/160	Art.-No. 531803
	or alternatively	
	FHD 12/200/330	Art.-No. 546597
	Hammer drilling with or without suction	

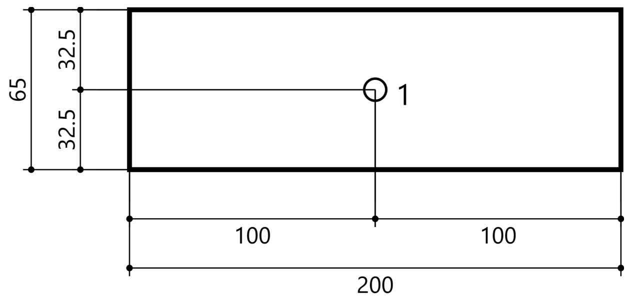
Installation details



Thread diameter	M 10
Drill hole diameter	d_0 = 12 mm
Drill hole depth	h_2 = 69 mm
Calculated anchorage depth	h_{ef} = 60 mm
Drilling method	Hammer drilling
Drill hole cleaning	4 times blowing, 4 times brushing, 4 times blowing required activities according the given instruction in the approval No borehole cleaning required in case of using a hollow drill bit, e.g. fischer FHD.
Installation type	Push-through installation
Annular gap	Annular gap filled
Maximum torque	$T_{inst,max}$ = 20.0 Nm
Socket size	17 mm
Base plate thickness	t = 9 mm
Total fixing thickness Tfix,max	t_{fix} = 9 mm
Volume of resin per drill hole	6 ml/3 scale divisions

Base plate details

Base plate material	Not available
Base plate thickness	t = 9 mm
Clearance hole in base plate	d_f=14 mm



Attachment

Profile type	None

Anchor coordinates

Anchor no.	x mm	y mm
1	0	0